

The Third Spectrum of Tantalum (Ta III): Fine and Hyperfine Structure

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Abstract

Presented is the first successful analysis of the Ta III spectrum. All the 37 levels of the low lying even configurations $5d^3$, $5d^26s$, and $5d6s^2$, and all the 68 levels of the higher odd configurations $5d^26p$ and $5d6s6p$ have been established. About 720 spectral lines have been classified in the region of $1000\text{--}3950\text{\AA}$ as belonging to the $(5d^3 + 5d^26s + 5d6s^2) - (5d^26p + 5d6s6p)$ transition array. The results are mainly based on spectrograms obtained by means of a vacuum sliding spark discharge and a 10.7 m normal incidence spectrograph at the Paris-Meudon Observatory, which provides a unique plate factor of 0.25\AA/mm in the first order. The resulting line list has been completed by partial data taken from earlier lists used for the Ta II and Ta IV studies. The analysis was guided by predicted energy level values and transition probabilities calculated by means of a complete set of orthogonal operators. The program suite IDEN for computer-aided spectra analyses played a crucial role in the study.

The list of classified spectral lines and derived energy level values are presented. Calculated energy values and Landé factors, LS -compositions and gA -values, obtained from the final fitted parameter values using the orthogonal operator approach are also given.

A few lines have partially resolved hyperfine structures owing to the high dispersion of the Meudon spectrograph. They connect levels with an unpaired $6s$ electron. The iso-nuclear trends of the a_{6s} hfs parameter are straight from Ta I to Ta III.

1. Introduction

Thanks to observations by the Goddard High Resolution Spectrograph (GHRS) on board the Hubble Space Telescope (HST) lines belonging to the spectra of 5d-elements have been identified in the chemically peculiar stars κ Cancri and χ Lupi [1]. It concerns especially the lower stages of ionization. As reported in the results of the “ χ Lupi Pathfinder Project” [2], abundances of Pt, Au and Hg in the star are 4–5 orders of magnitude higher than solar abundances. This renewed the interest for other 5d elements including tantalum.

The Ta III spectrum was the last third spectrum of all the non-radioactive elements left to be still unraveled. While the second, fourth, fifth and sixth tantalum spectra have been successfully studied in 1961–1978 [3–6], and the $5d5f - 5d^2$ array has been recently classified in Ta IV [7], all attempts to establish the structure of any configuration of Ta III failed. Some lines from the list used for the Ta IV analysis [4] were tentatively attributed to Ta III. Furthermore, the spark spectrum measured by C. C. Kiess in the Ta II study [3] contains many unidentified lines that could

belong to Ta III. Therefore, its analysis appeared as a stimulating challenge and deserved new experimental data and the support of improved theoretical tools.

2. Experimental

The spectrum of Ta has been recorded in the $1200\text{--}2450\text{\AA}$ wavelength region on the 10.7 m VUV normal incidence spectrograph at the Paris-Meudon Observatory. This instrument is equipped with a 3600 lines/mm holographic grating and provides a unique plate factor of 0.25\AA/mm in the first order [8]. The ionized tantalum spectrum in emission was obtained using a vacuum sliding spark source with an anode made of a 99.9% pure tantalum rod. A $10\text{ }\mu\text{F}$ capacitor was charged with a high voltage power supply delivering a voltage of 8 kV . To vary the discharge conditions, a self-inductance coil was placed in series with the spark source. For each wavelength region, two exposures were recorded with two values of the inductance, $68\text{ }\mu\text{H}$ and $25\text{ }\mu\text{H}$ in order to create “low” and “high” excitation conditions enhancing respectively lower (Ta III and Ta IV) and higher (Ta V and Ta VI) ionization stage emission. The anode was wrapped by a small piece of pure copper foil. The copper lines were used as internal standards for reducing the spectrograms. The plates were measured on a semi-automatic comparator equipped with a photoelectric device and connected to a linear fringe-counter, giving the plate position to $\pm 1\text{ }\mu\text{m}$. The measurements have initially been reduced by means of O, C, Al, Cu and Ta IV lines present in the spectrograms. However, as explained in the next section, the precision of wavelengths can be improved during the course of analysis by considering their overall consistency. The final relative accuracy of the wavelengths is 0.004\AA in the $1200\text{--}2445\text{\AA}$ region. Above 2445\AA and below 1200\AA the unidentified lines from Kiess [3] and one of us [9] were used respectively. The spectrograms from Ref. [9] were originally obtained for the Ta IV study [4] with the 6.65 m normal incidence vacuum spectrograph at the Zeeman laboratory, University of Amsterdam, The Netherlands, equipped with a 1200 lines/mm grating. The accuracy of the lines above 2445\AA is about 0.017\AA . All the identified spectral lines were weighted according to their accuracy before they were used in the calculation of the energy level system. The calculation procedure is able to detect systematic errors in

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wavelengths of spectral lines used. Our analysis showed that the lines from Ref. [9] have a systematic error of 0.013 Å with an additional random component of 0.010 Å.

3. Parametric calculations

Energy parameter values obtained in neighboring spectra were used to estimate starting parameter values for the Ta III calculations. Recently, a careful consideration of trends of energy parameter values along the Yb I isoelectronic sequence with the 5d² ground-state configuration was given [10]. The study showed quite regular evolution of the experimental parameters (or scaling factors of their *ab initio* values) along the sequence. Similar behavior was expected in the Lu I isoelectronic sequence, which consists of the ions having the 5d³ ground-state configuration and includes doubly ionized tantalum, Ta III. Some ions in the sequence have already been studied, viz. W IV, Re V, Os VI and Ir VII [11–15], thus providing a good starting point for the current analysis. It should be noticed that when the ionization stage lowers, the trends of parameters (or scaling factors of their *ab initio* values) become more irregular [10,16,17]. For instance, the mentioned factors for electrostatic parameters fall down sharply when we approach the third and second spectra. Also, the spectra of the lower stages of ionization are much more complex due to overlapping configurations in the even as well as in the odd system [17,18]. This, in part, is the reason why the Ta III spectrum has a long history of unsuccessful attempts to study.

The *ab initio* values of parameters needed for the purposes of extrapolation and estimation of starting parameter values for Ta III were calculated using the program developed by Cowan [19]. Calculations of energy level values and their eigenvector compositions were carried out by means of the orthogonal operator technique [16,20,21]. In these calculations the even system contained the 5d³, 5d²6s and 5d6s² configurations, and the odd system included the 5d²6p, 5d6s6p and 6s²6p configurations.

4. Computer aided analysis

The key instrument used in the analysis was the program suite IDEN [22,23]. A breakthrough was achieved by utilizing its module for the automatic search for energy levels. Input data for the code are lists of spectral lines, calculated energy levels and transition probabilities. Also specified are error bars for all the measured and all the calculated quantities, such as line wavelengths, energy level values and transition probabilities. Error bars for wavelengths may be given for separate lines and/or for parts of the line list. Random, as well as systematic errors may be specified. Moreover, one can specify a variety of constraints. Among them are the following:

(i) Correlation of wavelength measurements. The error bars of the measured wavelength of a spectral line may consist of a specified systematic fraction and a random fraction. Obviously, a value of the interval between two very close but isolated spectral lines has an error derived only from the random errors of the two lines. The systematic fraction of the resulting error of the

calculated interval is then equal to zero. On the contrary, for distant, not correlated lines we have to combine systematic errors of both lines to form the resulting systematic error of the interval. To take this into account in calculations, we also give a maximal interval of correlation for a specified systematic error. In our code a list of pairs “systematic error—maximal interval of correlation” may be specified for any and each part of the wavelength list. The systematic error of the distance between two lines is calculated as a function of the distance. The parameters of the function are determined by the relevant specified pairs “systematic error—maximal interval of correlation”.

(ii) Correlation of calculated energy levels. This is very important for calculation of error bars of intervals between energy levels. The error bars of the interval between two calculated levels may differ significantly depending on whether the levels belong to the same or different terms, to the same or different configurations. For example, the interval between two levels of a term of a configuration may be predicted with very high accuracy, though the configuration itself may be predicted with quite large uncertainty. This is because splitting of levels in a term, splitting of terms in a configuration and the average energy of the configuration are described by different parameters known with different accuracy. We have developed a simple way for specifying the whole error matrix reflecting correlation of all pairs of levels of the system under consideration.

The IDEN code first constructs a database and fills it with spectral lines pertinent for each allowed transition in accordance with the calculated transition probability, observed intensity, wavelength and other characteristics of lines, energy values of two levels involved, and also error bars specified for all these values. Then it performs reduction of the database (line selection, recalculation of error bars, etc.) by applying all the constraints that are intrinsic for the model, as well as all those that are specified. To speed up the process, a specially designed algorithm is used to apply the constraints in an optimal sequence. The current state of the problem solution can be examined in several ways. For example, the user may pick up the most developed transitions or levels, such as (a) those that contain the minimal number of possible variants of identification, e.g., with the least number of spectral lines pertinent for a transition, or (b) those that have minimal resulting (calculated after selection) error bars. Also, one may require to examine transitions or levels which are most sensitive to any changes in data or constraints related to them. Notable changes in such places will most probably result in significant changes in the data sets of other transitions/levels. During such a revision one may decide to change constraints or edit the data sets, e.g., edit a list of selected spectral lines for a transition. For instance, one may leave only one spectral line for a given transition and see if the whole system will survive the selection, i.e. if it will have at least one spectral line for each allowed transition. Initially we limit the automatic search by a set of levels connected by relatively strong calculated

transitions, introduce the constraints, and then gradually strengthen them in the course of an iterative procedure including database reduction and semiempirical recalculations of levels. Subsequently, moderate intensity transitions are added to the database. At the final stage we use the interactive routine of the IDEN suite to pick up the weakest spectral lines, to check identified lines having abnormally high intensity, to verify multiply identified and blended lines and to re-specify the wavelength accuracy for all these lines.

All the identified spectral lines were weighted according to their accuracy before they were used in the calculation of the energy level system. The calculation procedure is able to detect systematic errors in wavelengths of spectral lines used. Indeed, in the process of the analysis we found that our initially calculated wavelengths have regions with systematic deviations of up to 0.020 \AA . Those were regions poor of standard lines and/or regions close to the edges of the photographic plates. This leads us to revise the standards and either carefully remeasure them or discard them if blended or saturated. At the same time we added some secondary standards obtained from the analysis: for some identified isolated lines we used calculated wavelengths derived from the very well determined energy levels. After finishing level searching we extended our list of classified lines above 2445 \AA and below 1200 \AA . The unidentified lines from Kiess [3] and Ref. [9] were used for this purpose, respectively. Comparison of line intensities from Kiess [3] and on our spectrograms in the overlapping wavelength region provided a criterion for selecting unidentified lines from Ref. [3] for Ta III. Indeed, these lines are rather weaker than the identified Ta II lines whereas they are stronger on our plates.

5. Results and discussion

As a result of the analysis, in the region of 1009 – 3944 \AA , 724 spectral lines have been classified as belonging to the $(5d^3 + 5d^26s + 5d6s^2) - (5d^26p + 5d6s6p)$ transition array of Ta III. Nine lines are doubly classified. All identified lines and their classifications are given in Table I. In the first column of this table we give the theoretical transition probability, gA , for each identified transition. The second column shows the intensity of the spectral lines (Int) on a scale 1–250. The weakest spectral line detectable on Meudon's plates on the scale given is about 0.5. As can be seen, the agreement between gA and Int for the isolated unperturbed lines is quite good. The third, fourth, fifth and sixth columns show wavelength, wavenumber, and two differences: between the experimental and calculated (by using the experimental energies of the levels involved) wavenumbers and wavelengths. Next two columns, viz. seventh (N_{even}) and eighth (N_{odd}), give information about the even and odd levels involved in the transition: the number of identified spectral lines used to determine the level. In the ninth and tenth columns we give the names of the configurations and energy values for the even and odd levels involved in the transition, respectively. For the even levels the names of the levels are also given. For the odd levels the J -values of the levels are shown in brackets. The last column contains remarks. Lines marked by “c” and “d” in this column are respectively from Ref. [9] and Ref.

[3] As can be seen from Table I, the finally achieved relative accuracy of wavelengths in the main list (1204 – 2445 \AA) is 0.004 \AA . The accuracy of the lines above 2445 \AA [3] is about 0.017 \AA . Lines below 1200 \AA [9] have a systematic error of 0.013 \AA with an additional random component of 0.010 \AA . One may notice in Table I twelve pairs of close lines which, due to the large dispersion of the spectrograph, exhibit resolved hyperfine structures (see next section).

All the 37 levels of the $5d^3$, $5d^26s$ and $5d6s^2$ configurations and all the 68 levels of the $5d^26p$ and $5d6s6p$ configurations have been established. The even levels are determined by 4–39 (by 19 in average) transitions. The odd levels are based on 2–18 (on 11 in average) spectral lines. These numbers show that the reliability of the analysis is quite high. Experimental and calculated energy values of the even parity levels in the $5d^3$, $5d^26s$ and $5d6s^2$ configurations and the odd parity levels in the $5d^26p$, $5d6s6p$ and $6s^26p$ configurations of Ta III are given respectively in Table II and Table III. The first three columns of the tables show the observed and calculated energy values of levels and also the difference between these values. In the fourth column we give the number of identified spectral lines used to determine the level. The fifth column lists the root-mean-squares (rms) deviation of the energy values calculated from wavenumbers by excluding masked, blended and multiply identified lines. The calculated Landé factors, g , of levels are given in the sixth column. In the last columns of the two tables the compositions of eigenvectors are given. In the odd system many main components are below 50%, with the lowest being 19%. Due to the strong level mixing, the LS -notation for odd levels have not been given in Table I. The uncertainty in the adopted energy values of the 102 established levels is 0.05 – 0.16 cm^{-1} , and does not exceed 0.10 cm^{-1} for 90% of them. Only three levels are determined with a rms deviation of 0.20 – 0.30 cm^{-1} .

All the semiempirical calculations (fitting) were carried out by using the orthogonal operator technique [16,20,21]. Some parameters of the studied configurations, all the parameters of the unknown configuration $6s^26p$ and also three configuration interaction parameters in the odd system were kept fixed at the predetermined values during the fitting procedure. In Table IV and Table V the parameters obtained (or used fixed) in the calculations for the even and odd systems are presented. The second columns of the tables show the parameter values obtained in the final least-squares fit (LSF). Values in brackets are the uncertainties of the fitted parameter values. In the third columns the *ab initio* values of the parameters calculated using the Hartree–Fock method with relativistic correction (HFR) [19] are presented. The obtained (or predetermined and fixed) scaling factors (LSF/HFR) are shown in the forth columns of Table IV and Table V.

6. Hyperfine structure

As mentioned before, twelve hyperfine structures can be seen in Table I. Natural tantalum, of which our light source is made, is almost pure ^{181}Ta isotope (99.978%) with a nuclear spin $I = 7/2$ and a nuclear magnetic moment $\mu = 2.3\text{ nm}$. In the case of neutral tantalum (Ta I) studied with atomic beam LIF techniques, lines exhibit hyperfine

Table I. Classified lines in the $(5d^3 + 5d^26s + 5d6s^2) - (5d^26p + 5d6s6p)$ transition array of Ta III.

$g_A^{(A)}$ (10^3 s $^{-1}$)	Int	λ (Å)	v (cm $^{-1}$)	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark
13	20	1009.517	99057.30	-2.00	0.020	28	9	5d 3	$^2P_{3/2}$	7186.97
2	25	1012.072	98807.18	-1.37	0.014	17	10	5d 3	$^4F_{5/2}$	2512.43
14	14	1072.044	93279.74	-1.72	0.020	13	6	5d 3	$^2P_{1/2}$	7882.85
77	13	1121.246	89186.52	-0.08	0.001	39	10	5d 3	$^3D_{5/2}$	12134.38
20	1	1130.551	88452.44	-1.59	0.020	28	13	5d 3	$^2P_{3/2}$	7186.97
17	2	1132.068	88333.92	-1.99	0.026	28	13	5d 2 6s (3F)	$^4F_{5/2}$	7305.09
47	19	1133.331	88235.44	-0.51	0.006	39	10	5d 3	$^3D_{5/2}$	12134.38
21	14	1169.830	85482.54	-0.67	0.009	26	6	5d 3	$^4P_{3/2}$	15681.10
145	74	1181.330	84650.32	-0.16	0.002	33	10	5d 2 6s (3F)	$^2F_{5/2}$	15719.85
10	80	1192.669	83845.55	-1.06	0.015	13	14	5d 3	$^2P_{1/2}$	7882.85
29	13	1197.333	83518.94	-1.19	0.017	15	10	5d 3	$^2H_{9/2}$	17800.85
43	37	1197.507	83506.79	0.17	-0.002	39	13	5d 3	$^3D_{5/2}$	12134.38
216	57	1198.836	83414.25	-0.09	0.001	29	10	5d 2 6s (3F)	$^2F_{7/2}$	17906.64
61	49	1199.490	83368.77	-2.32	0.033	23	12	5d 3	$^3D_{3/2}$	12626.87
27	9	1204.612	83014.28	0.15	-0.002	23	13	5d 3	$^3D_{3/2}$	12626.87
329	85	1212.657	82463.55	-0.14	0.002	29	10	5d 2 6s (3F)	$^2F_{7/2}$	17906.64
16	1	1225.001	81632.59	0.19	-0.003	32	12	5d 3	$^4P_{5/2}$	14365.56
6	1	1225.580	81594.02	0.20	-0.003	16	11	5d 3	$^4F_{3/2}$	0.0
52	32	1230.381	81275.64	0.20	-0.003	32	13	5d 3	$^4P_{5/2}$	14365.56
5	1	1232.160	81158.29	0.18	-0.003	27	9	5d 2 6s (3F)	$^4F_{3/2}$	5542.39
65	23	1245.069	80316.83	-0.03	0.000	26	12	5d 3	$^4P_{3/2}$	15681.10
57	37	1245.669	80278.15	0.04	-0.001	33	12	5d 2 6s (3F)	$^2F_{5/2}$	15719.85
220	53	1251.233	79921.17	0.02	0.000	33	13	5d 2 6s (3F)	$^2F_{5/2}$	15719.85
39	1	1256.360	79595.02	-0.06	0.001	39	14	5d 3	$^3D_{5/2}$	12134.38
7	53	1257.656	79513.02	-0.51	0.008	28	9	5d 3	$^2P_{3/2}$	7186.97
79	18	1259.575	79391.84	0.21	-0.003	24	9	5d 3	$^2F_{5/2}$	26854.64
52	45	1264.177	79102.82	0.23	-0.004	23	14	5d 3	$^3D_{3/2}$	12626.87
314	64	1280.551	78091.38	0.05	-0.001	29	12	5d 2 6s (3F)	$^2F_{7/2}$	17906.64
47	5	1284.716	77838.20	0.12	-0.002	19	9	5d6s 2	$^2D_{3/2}$	28408.19
24	43	1290.337	77499.13	-0.57	0.010	39	6	5d 3	$^3D_{5/2}$	12134.38
5	1	1290.726	77475.77	-0.06	0.001	28	10	5d 3	$^2P_{3/2}$	7186.97
31	2	1292.592	77363.94	0.04	-0.001	32	14	5d 3	$^4P_{5/2}$	14365.56
7	8	1302.424	76779.92	-0.03	0.001	13	10	5d 3	$^2P_{1/2}$	7882.85
25	39	1314.445	76077.73	-0.27	0.005	39	14	5d 3	$^3D_{5/2}$	12134.38
6	5	1314.909	76050.88	-0.56	0.010	27	11	5d 2 6s (3F)	$^4F_{3/2}$	5542.39
43	50	1314.956	76048.16	-0.20	0.003	26	14	5d 3	$^4P_{3/2}$	15681.10
157	23	1315.622	76009.67	0.06	-0.001	33	14	5d 2 6s (3F)	$^2F_{5/2}$	15719.85
8	5	1323.003	75585.59	0.08	-0.002	23	14	5d 3	$^3D_{3/2}$	12626.87
26	3	1323.820	75538.97	-0.49	0.009	24	10	5d 2 6s (1D)	$^2D_{5/2}$	25781.52
149	53	1340.689	74588.49	-0.32	0.006	24	10	5d 2 6s (1D)	$^2D_{5/2}$	25781.52
15	6	1341.094	74566.00	-0.12	0.002	39	9	5d 3	$^3D_{5/2}$	12134.38
140	41	1342.893	74466.07	-0.27	0.005	24	10	5d 3	$^2F_{5/2}$	26854.64
18	18	1343.966	74406.64	-0.21	0.004	28	11	5d 3	$^2P_{3/2}$	7186.97
11	1	1346.095	74288.98	0.25	-0.005	28	11	5d 2 6s (3F)	$^4F_{5/2}$	7305.09
455	68	1348.029	74182.41	-0.05	0.001	18	9	5d6s 2	$^2D_{5/2}$	32063.81
721	64	1351.516	73990.97	-0.39	0.007	13	10	5d 2 6s (1G)	$^2G_{9/2}$	27329.62
27	31	1352.909	73914.81	0.58	-0.011	33	6	5d 2 6s (3F)	$^2F_{5/2}$	15719.85
412	60	1360.261	73515.31	-0.38	0.007	24	10	5d 3	$^2F_{5/2}$	26854.64
130	8	1362.424	73398.60	-0.49	0.009	19	10	5d 2 6s (1G)	$^2G_{7/2}$	26971.24
38	2	1364.391	73292.77	-0.14	0.003	10	9	5d 2 6s (3P)	$^2P_{1/2}$	32953.36
15	1	1364.536	73284.96	-0.65	0.012	15	7	5d 3	$^4F_{9/2}$	6776.24
7	7	1365.065	73256.61	-0.45	0.008	27	7	5d 2 6s (3F)	$^4F_{3/2}$	5542.39
12	25	1374.152	72772.15	0.38	-0.007	27	13	5d 2 6s (3F)	$^4F_{7/2}$	10425.17
265	73	1374.456	72756.07	-0.05	0.001	19	6	5d6s 2	$^2D_{3/2}$	28408.19
18	11	1378.711	72531.52	0.24	-0.004	26	14	5d 3	$^4P_{3/2}$	15681.10
39	34	1379.454	72492.47	-0.06	0.001	33	14	5d 2 6s (3F)	$^2F_{5/2}$	15719.85
5	2	1382.463	72334.67	-0.27	0.005	32	9	5d 3	$^4P_{5/2}$	14365.56
20	10	1385.008	72201.73	0.04	-0.001	22	12	5d 2 6s (1D)	$^2D_{3/2}$	23796.27
2	1	1386.313	72133.77	0.04	-0.001	17	12	5d 3	$^4F_{5/2}$	2512.43
424	73	1389.940	71945.57	0.06	-0.001	18	10	5d 3	$^2F_{7/2}$	29375.47
3	23	1391.651	71857.10	-0.14	0.003	10	10	5d 3	$^4P_{1/2}$	12805.56
106	85	1391.888	71844.88	0.14	-0.003	22	13	5d 2 6s (1D)	$^2D_{3/2}$	23796.27
8	92	1392.115	71833.16	-0.07	0.001	15	6	5d 3	$^2H_{9/2}$	17800.85
43	2	1394.162	71727.70	0.25	-0.005	29	6	5d 2 6s (3F)	$^2F_{7/2}$	17906.64
21	92	1398.710	71494.43	0.07	-0.001	28	7	5d 2 6s (3F)	$^4F_{5/2}$	7305.09
16	25	1399.283	71465.18	0.25	-0.005	28	12	5d 2 6s (3F)	$^4F_{5/2}$	7305.09
41	68	1407.204	71062.89	0.33	-0.006	39	13	5d 3	$^2D_{5/2}$	12134.38
16	37	1407.277	71059.22	0.37	-0.007	28	9	5d 3	$^2P_{3/2}$	7186.97
976	92	1408.549	70995.05	0.19	-0.004	18	10	5d 3	$^2F_{7/2}$	29375.47
8	6	1409.022	70971.23	0.36	-0.007	15	4	5d 3	$^4F_{9/2}$	6776.24
10	10	1415.445	70649.15	-0.26	0.005	17	18	5d 3	$^4F_{5/2}$	2512.43
8	21	1417.902	70526.75	-0.12	0.002	18	14	5d 3	$^4F_{7/2}$	4854.18
3	10	1421.950	70325.97	0.07	-0.002	18	9	5d 3	$^4F_{7/2}$	4854.18
16	3	1422.360	70305.69	-0.05	0.001	29	14	5d 2 6s (3F)	$^2F_{7/2}$	17906.64
11	53	1433.725	69748.36	-0.33	0.007	28	17	5d 3	$^2P_{3/2}$	7186.97
443	67	1433.757	69746.84	0.24	-0.005	14	9	5d 2 6s (3P)	$^2P_{3/2}$	36499.67
24	21	1435.346	69669.61	0.05	-0.001	14	9	5d 2 6s (3P)	$^4P_{1/2}$	17030.94

Table I. *Continued.*

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark
44	73	1436.022	69636.80	0.13	-0.003	27	7	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
2	9	1436.614	69608.11	-0.05	0.001	27	4	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39
22	16	1440.192	69435.21	0.24	-0.005	23	14	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41
856	90	1443.890	69257.34	0.17	-0.004	18	10	$5d6s^2$	$^2D_{5/2}$	32063.81
1	3	1445.956	69158.38	0.22	-0.005	27	13	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
44	61	1446.275	69143.14	-0.18	0.004	24	12	$5d^3$	$^2F_{5/2}$	26854.64
25	26	1446.567	69129.20	0.12	-0.003	18	13	$5d^3$	$^4F_{7/2}$	4854.18
16	25	1447.096	69103.93	0.16	-0.003	27	12	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39
926	90	1448.710	69026.91	0.19	-0.004	19	12	$5d^26s$ (1G)	$^2G_{7/2}$	26971.24
9	73	1449.668	68981.30	-0.40	0.008	26	10	$5d^3$	$^4P_{3/2}$	15681.10
84	81	1449.971	68966.91	-0.04	0.001	23	11	$5d^3$	$^2D_{3/2}$	12626.87
5	16	1452.818	68831.76	0.38	-0.008	32	13	$5d^3$	$^4P_{5/2}$	14365.56
116	61	1453.774	68786.46	0.10	-0.002	24	13	$5d^3$	$^2F_{5/2}$	26854.64
9	40	1454.219	68765.45	-0.30	0.006	22	7	$5d^3$	$^2G_{7/2}$	11296.10
11	20	1454.679	68743.67	0.15	-0.003	15	7	$5d^3$	$^4F_{9/2}$	6776.24
8	14	1454.945	68731.13	0.01	0.000	16	15	$5d^3$	$^4F_{3/2}$	0.0
15	57	1457.622	68604.89	0.08	-0.002	15	14	$5d^3$	$^4F_{9/2}$	6776.24
3	9	1459.720	68506.27	0.04	-0.001	16	14	$5d^3$	$^4F_{3/2}$	0.0
20	61	1463.167	68344.91	0.06	-0.001	27	12	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
22	40	1463.965	68307.64	-0.02	0.000	18	18	$5d^3$	$^4F_{7/2}$	4854.18
167	81	1463.982	68306.84	0.32	-0.007	18	10	$5d6s^2$	$^2D_{5/2}$	32063.81
205	57	1466.038	68211.05	0.10	-0.002	10	6	$5d^26s$ (3P)	$^2P_{1/2}$	32953.36
37	49	1466.318	68198.02	-0.01	0.000	27	10	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
24	73	1468.222	68109.58	0.15	-0.003	25	14	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95
4	3	1470.914	67984.93	-0.05	0.001	16	12	$5d^3$	$^4F_{3/2}$	0.0
73	43	1472.035	67933.19	0.00	0.000	22	14	$5d^26s$ (1D)	$^2D_{3/2}$	23796.27
68	67	1473.297	67874.96	-0.03	0.001	28	9	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09
19	43	1476.853	67711.55	-0.04	0.001	17	7	$5d^3$	$^2G_{9/2}$	12350.26
6	1	1478.594	67631.82	-0.04	0.001	14	10	$5d^26s$ (3P)	$^4P_{1/2}$	17030.94
4	2	1478.866	67619.38	-0.08	0.002	27	18	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39
814	90	1479.517	67589.64	-0.13	0.003	19	12	$5d6s^2$	$^2D_{3/2}$	28408.19
36	49	1481.356	67505.73	-0.20	0.005	22	4	$5d^26s$ (1D)	$^2D_{3/2}$	23796.27
33	34	1481.985	67477.09	0.00	0.000	33	13	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85
9	7	1482.055	67473.87	-0.05	0.001	22	12	$5d^3$	$^2G_{7/2}$	11296.10
6	16	1482.604	67448.90	-0.05	0.001	39	13	$5d^3$	$^2D_{5/2}$	12134.38
4	22	1484.119	67380.05	-0.10	0.002	27	15	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
170	73	1487.370	67232.76	-0.05	0.001	19	13	$5d6s^2$	$^2D_{3/2}$	28408.19
8	26	1487.944	67206.84	-0.18	0.004	15	13	$5d^3$	$^4F_{9/2}$	6776.24
11	6	1492.086	67020.27	-0.09	0.002	27	6	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39
4	9	1493.509	66956.40	-0.06	0.001	23	13	$5d^3$	$^2D_{3/2}$	12626.87
7	9	1493.692	66948.20	-0.04	0.001	18	15	$5d^3$	$^4F_{7/2}$	4854.18
2	2	1494.206	66925.20	-0.22	0.005	17	16	$5d^3$	$^4F_{5/2}$	2512.43
11	73	1495.110	66884.73	0.01	0.000	17	12	$5d^3$	$^4F_{5/2}$	2512.43
52	67	1497.829	66763.29	-0.02	0.001	13	12	$5d^3$	$^2P_{1/2}$	7882.85
48	73	1499.745	66678.01	-0.16	0.004	28	13	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09
45	40	1500.039	66664.95	-0.12	0.003	39	7	$5d^3$	$^2D_{5/2}$	12134.38
24	67	1500.524	66643.40	-0.15	0.003	27	6	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39
69	73	1500.701	66635.55	-0.09	0.002	39	12	$5d^3$	$^2D_{5/2}$	12134.38
15	4	1501.555	66597.65	0.10	-0.002	25	9	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95
49	67	1503.548	66509.33	0.11	-0.003	22	15	$5d^3$	$^2G_{7/2}$	11296.10
1	4	1507.657	66328.08	0.02	0.000	16	8	$5d^3$	$^4F_{3/2}$	0.0
3	3	1508.056	66310.52	0.04	-0.001	16	13	$5d^3$	$^4F_{3/2}$	0.0
472	101	1508.393	66295.73	0.01	0.000	14	7	$5d^26s$ (3F)	$^4F_{9/2}$	13766.13
59	67	1508.909	66273.03	0.09	-0.002	17	10	$5d^3$	$^2G_{9/2}$	12350.26
8	8	1510.148	66218.66	-0.02	0.001	17	15	$5d^3$	$^4F_{5/2}$	2512.43
20	3	1511.871	66143.20	0.05	-0.001	23	12	$5d^3$	$^2D_{3/2}$	12626.87
15	90	1512.600	66111.32	-0.12	0.003	39	9	$5d^3$	$^2D_{5/2}$	12134.38
16	29	1515.729	65974.84	-0.03	0.001	28	18	$5d^3$	$^2P_{3/2}$	7186.97
51	30	1516.346	65947.99	0.05	-0.001	24	14	$5d^26s$ (1D)	$^2D_{5/2}$	25781.52
13	21	1517.158	65912.73	0.01	0.000	26	11	$5d^3$	$^4P_{3/2}$	15681.10
7	5	1518.445	65856.84	0.09	-0.002	28	18	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09
32	3	1520.321	65775.56	0.06	-0.001	6	9	$5d^3$	$^2D_{3/2}$	40470.77
5	38	1522.741	65671.05	0.12	-0.003	39	15	$5d^3$	$^2D_{5/2}$	12134.38
4	5	1523.469	65639.66	0.10	-0.002	22	17	$5d^3$	$^2G_{7/2}$	11296.10
42	81	1523.994	65617.06	0.04	-0.001	15	11	$5d^3$	$^4F_{9/2}$	6776.24
13	20	1527.760	65455.30	0.24	-0.006	17	15	$5d^3$	$^2G_{9/2}$	12350.26
7	10	1528.111	65440.27	0.01	0.000	10	9	$5d^3$	$^4P_{1/2}$	12805.56
5	7	1531.619	65290.37	0.07	-0.002	29	13	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64
8	16	1533.324	65217.80	0.03	-0.001	32	13	$5d^3$	$^4P_{5/2}$	14365.56
119	67	1537.843	65026.14	-0.04	0.001	15	15	$5d^3$	$^4F_{9/2}$	6776.24
7	25	1538.487	64998.93	-0.04	0.001	28	6	$5d^3$	$^2P_{3/2}$	7186.97
142	73	1541.287	64880.84	-0.01	0.000	28	6	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09
126	32	1541.429	64874.86	0.04	-0.001	24	14	$5d^3$	$^2F_{5/2}$	26854.64
570	81	1541.852	64857.07	0.00	0.000	14	10	$5d^26s$ (3F)	$^4F_{9/2}$	13766.13
8	40	1543.180	64801.27	-0.01	0.000	39	17	$5d^3$	$^2D_{5/2}$	12134.38
423	81	1544.284	64754.93	0.02	-0.001	27	9	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
77	12	1546.440	64664.64	0.00	0.000	14	6	$5d^26s$ (3P)	$^2P_{3/2}$	36499.67

Table I. Continued.

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark	
20	43	1547.486	64620.93	-0.14	0.003	27	10	$5d^26s (^3F)$	$4F_{3/2}$	5542.39	
4	21	1548.382	64583.53	-0.13	0.003	18	16	$5d^3$	$4F_{7/2}$	4854.18	
34	61	1549.356	64542.96	-0.01	0.000	18	12	$5d^3$	$4F_{7/2}$	4854.18	
14	49	1550.452	64497.33	0.00	0.000	28	15	$5d^26s (^3F)$	$4F_{5/2}$	7305.09	
35	43	1551.094	64470.63	-0.05	0.001	28	13	$5d^3$	$2P_{3/2}$	7186.97	
47	26	1551.978	64433.91	0.02	0.000	32	7	$5d^3$	$4P_{5/2}$	14365.56	
67	53	1552.323	64419.57	0.04	-0.001	23	13	$5d^26s (^3P)$	$4P_{3/2}$	18777.41	
40	34	1552.409	64416.03	-0.08	0.002	22	14	$5d^26s (^1D)$	$2D_{3/2}$	23796.27	
57	36	1552.687	64404.48	0.02	0.000	32	12	$5d^3$	$4P_{5/2}$	14365.56	
126	36	1553.939	64352.58	0.02	-0.001	28	13	$5d^26s (^3F)$	$4F_{5/2}$	7305.09	
11	67	1554.984	64309.32	0.53	-0.013	23	17	$5d^3$	$2D_{3/2}$	12626.87	
50	57	1557.059	64223.64	-0.01	0.000	22	7	$5d^3$	$2G_{7/2}$	11296.10	
1	5	1561.192	64053.63	0.06	-0.002	16	17	$5d^3$	$4F_{3/2}$	0.0	
200	73	1561.544	64039.18	-0.01	0.000	14	15	$5d^26s (^3F)$	$4F_{9/2}$	13766.13	
115	73	1563.102	63975.34	-0.10	0.003	27	4	$5d^26s (^3F)$	$4F_{3/2}$	5542.39	
46	5	1564.111	63934.09	-0.06	0.001	18	12	$5d6s^2$	$2D_{5/2}$	32063.81	
15	36	1564.891	63902.23	0.00	0.000	26	13	$5d^3$	$4P_{3/2}$	15681.10	
65	61	1565.340	63883.89	-0.09	0.002	22	9	$5d^3$	$2G_{7/2}$	11296.10	
176	40	1565.670	63870.44	-0.22	0.006	14	10	$5d^26s (^3P)$	$2P_{3/2}$	36499.67	
163	90	1565.841	63863.45	-0.03	0.001	33	13	$5d^26s (^3F)$	$2F_{5/2}$	15719.85	
31	53	1567.449	63797.92	-0.13	0.003	17	13	$5d^3$	$4F_{5/2}$	2512.43	
7	5	1568.019	63774.76	-0.04	0.001	13	13	$5d^3$	$2P_{1/2}$	7882.85	
12	2	1571.043	63651.97	-0.08	0.002	18	14	$5d^3$	$4F_{7/2}$	4854.18	
297	40	1571.666	63626.75	0.01	0.000	4	9	$5d^3$	$2D_{5/2}$	42619.53	
258	49	1572.893	63577.10	-0.09	0.002	18	13	$5d6s^2$	$2D_{5/2}$	32063.81	
288	81	1573.369	63557.89	-0.20	0.005	27	13	$5d^26s (^3F)$	$4F_{7/2}$	10425.17	
24	36	1576.302	63439.61	-0.16	0.004	32	15	$5d^3$	$4P_{5/2}$	14365.56	
39	57	1578.460	63352.89	-0.06	0.002	16	14	$5d^3$	$4F_{3/2}$	0.0	
181	46	1579.249	63321.24	-0.03	0.001	19	14	$5d6s^2$	$2D_{3/2}$	28408.19	
19	53	1580.226	63282.09	-0.14	0.003	18	10	$5d^3$	$4F_{7/2}$	4854.18	
48	21	1581.114	63246.54	-0.13	0.003	39	14	$5d^3$	$2D_{5/2}$	12134.38	
88	16	1581.886	63215.68	-0.07	0.002	27	8	$5d^26s (^3F)$	$4F_{3/2}$	5542.39	
28	53	1582.565	63188.56	-0.16	0.004	27	15	$5d^26s (^3F)$	$4F_{3/2}$	5542.39	
74	57	1583.044	63169.43	-0.07	0.002	17	7	$5d^3$	$2G_{9/2}$	12350.26	
89	61	1584.937	63093.98	-0.01	0.000	25	13	$5d^26s (^3P)$	$4P_{5/2}$	20102.95	
6	5	1585.056	63089.25	0.33	-0.008	26	12	$5d^3$	$4P_{3/2}$	15681.10	
36	61	1586.040	63050.13	-0.05	0.001	33	12	$5d^26s (^3F)$	$2F_{5/2}$	15719.85	
184	67	1586.526	63030.78	-0.01	0.000	17	14	$5d^3$	$2G_{9/2}$	12350.26	
14	40	1587.901	62976.21	-0.28	0.007	28	10	$5d^3$	$2P_{3/2}$	7186.97	
203	22	1588.148	62966.44	0.00	0.000	4	9	$5d^26s (^1S)$	$2S_{1/2}$	43279.83	
203	34	1588.204	62964.19	-0.09	0.002	4	9	$5d^26s (^1S)$	$2S_{1/2}$	43281.99	
42	34	1589.719	62904.20	-0.03	0.001	22	9	$5d^26s (^1D)$	$2D_{3/2}$	23796.27	
97	43	1589.973	62894.15	0.14	-0.003	19	4	$5d6s^2$	$2D_{3/2}$	28408.19	
151	73	1590.875	62858.47	0.10	-0.003	28	10	$5d^26s (^3F)$	$4F_{5/2}$	7305.09	
259	90	1593.961	62736.77	0.10	-0.003	27	18	$5d^26s (^3F)$	$4F_{7/2}$	10425.17	
75	81	1595.222	62687.21	0.05	-0.001	22	13	$5d^3$	$2G_{7/2}$	11296.10	
46	22	1595.843	62662.80	-0.04	0.001	19	6	$5d^26s (^1G)$	$2G_{7/2}$	26971.24	
51	57	1598.205	62570.20	0.09	-0.002	32	17	$5d^3$	$4P_{5/2}$	14365.56	
95	61	1599.394	62523.66	-0.02	0.000	23	4	$5d^3$	$2D_{3/2}$	12626.87	
14	61	1601.468	62442.73	0.14	-0.004	27	12	$5d^26s (^3F)$	$4F_{3/2}$	5542.39	
356	67	1601.772	62430.87	0.01	0.000	24	14	$5d^26s (^1D)$	$2D_{5/2}$	25781.52	
6	49	1601.954	62423.75	0.08	-0.002	16	9	$5d^3$	$4F_{3/2}$	0.0	
10	53	1603.812	62351.45	0.05	-0.001	17	15	$5d^3$	$4F_{5/2}$	2512.43	
110	67	1604.340	62330.94	0.08	-0.002	28	4	$5d^3$	$2P_{3/2}$	7186.97	
1031	101	1605.023	62304.41	-0.05	0.001	13	6	$5d^26s (^1G)$	$2G_{9/2}$	27329.62	
22	32	1606.141	62261.03	0.03	-0.001	15	7	$5d^3$	$2H_{9/2}$	17800.85	
25	19	1606.401	62250.96	0.50	-0.013	14	2	$5d^26s (^3P)$	$4P_{1/2}$	17030.94	
22	1606.435	62249.64	-0.82	0.021						Hfs	
2	40	1607.455	62210.16	-0.02	0.001	28	12	$5d^3$	$2P_{3/2}$	7186.97	Hfs
11	14	1609.461	62132.60	-0.15	0.004	28	16	$5d^26s (^3F)$	$4F_{5/2}$	7305.09	
3	73	1610.511	62092.07	0.01	-0.001	28	12	$5d^26s (^3F)$	$4F_{5/2}$	7305.09	
11	21	1613.722	61968.53	0.44	-0.011	27	11	$5d^26s (^3F)$	$4F_{7/2}$	10425.17	
25	57	1616.000	61881.18	0.02	-0.001	17	15	$5d^3$	$4F_{5/2}$	2512.43	
17	36	1616.402	61865.78	0.04	-0.001	22	18	$5d^3$	$2G_{7/2}$	11296.10	
40	61	1616.844	61848.89	0.01	-0.001	39	13	$5d^3$	$2D_{5/2}$	12134.38	
14	34	1617.058	61840.70	0.10	-0.003	10	12	$5d^3$	$4P_{1/2}$	12805.56	
129	61	1618.947	61768.55	0.04	-0.001	14	7	$5d^26s (^3P)$	$4P_{1/2}$	17030.94	
234	67	1622.983	61614.93	0.01	0.000	14	14	$5d^26s (^3F)$	$4F_{9/2}$	13766.13	
5	10	1624.135	61571.24	0.07	-0.002	28	8	$5d^3$	$2P_{3/2}$	7186.97	
3	18	1624.931	61541.07	-0.06	0.002	17	17	$5d^3$	$4F_{5/2}$	2512.43	
29	49	1627.172	61456.33	0.03	-0.001	18	13	$5d^3$	$4F_{7/2}$	4854.18	
183	81	1627.968	61426.25	0.23	-0.006	28	15	$5d^26s (^3F)$	$4F_{5/2}$	7305.09	
61	90	1629.272	61377.11	-0.14	0.004	27	15	$5d^26s (^3F)$	$4F_{7/2}$	10425.17	
49	67	1629.721	61360.19	0.02	-0.001	15	10	$5d^3$	$4F_{9/2}$	6776.24	
42	25	1629.785	61357.78	0.04	-0.001	24	14	$5d^3$	$2F_{5/2}$	26854.64	
7	2	1630.812	61319.16	-0.10	0.003	28	14	$5d^3$	$2P_{3/2}$	7186.97	
48	49	1632.532	61254.55	-0.01	0.000	26	17	$5d^3$	$4P_{3/2}$	15681.10	

Table I. *Continued.*

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark
207	73	1632.891	61241.09	-0.05	0.001	19	14	$5d^26s (^1G)$	$^2G_{7/2}$ 26971.24	5d6s6p 88212.38(5/2)
19	49	1633.563	61215.89	0.09	-0.002	33	17	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	5d 26p 76935.66(5/2)
29	34	1633.957	61201.14	0.00	0.000	28	14	$5d^26s (^3F)$	$^4F_{5/2}$ 7305.09	5d 26p 68506.23(5/2)
4	4	1636.738	61097.12	-0.04	0.001	22	11	$5d^3$	$^2G_{7/2}$ 11296.10	5d 26p 72393.26(9/2)
10	14	1638.606	61027.49	0.03	-0.001	39	18	$5d^3$	$^2D_{5/2}$ 12134.38	5d 26p 73161.84(5/2)
29	34	1640.475	60957.94	0.04	-0.001	16	5	$5d^3$	$^4F_{3/2}$ 0.0	5d 26p 60957.90(1/2)
82	67	1641.523	60919.04	0.05	-0.002	24	9	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	5d6s6p 86700.50(3/2)
24	61	1642.699	60875.43	0.14	-0.004	13	8	$5d^3$	$^2P_{1/2}$ 7882.85	5d 26p 68758.14(1/2)
21	43	1642.936	60866.65	0.12	-0.003	22	10	$5d^26s (^1D)$	$^2D_{3/2}$ 23796.27	5d 26p 84662.80(1/2)
50	13	1643.017	60863.65	0.27	-0.007	29	12	$5d^26s (^3F)$	$^2F_{7/2}$ 17906.64	5d6s6p 78770.02(5/2)
1	5	1643.431	60848.33	0.07	-0.002	13	15	$5d^3$	$^2P_{1/2}$ 7882.85	5d 26p 68731.11(3/2)
129	90	1643.639	60840.59	0.06	-0.002	17	14	$5d^3$	$^4F_{5/2}$ 2512.43	5d 26p 63352.96(3/2)
180	81	1644.130	60822.46	0.11	-0.003	15	10	$5d^3$	$^2H_{9/2}$ 17800.85	5d6s6p 78623.20(7/2)
77	67	1644.342	60814.62	0.10	-0.003	32	9	$5d^3$	$^4P_{5/2}$ 14365.56	5d6s6p 75180.08(5/2)
65	81	1645.123	60785.72	0.05	-0.001	27	8	$5d^26s (^3F)$	$^4F_{3/2}$ 5542.39	5d6s6p 66328.06(3/2)
21	67	1645.598	60768.19	0.10	-0.003	27	13	$5d^26s (^3F)$	$^4F_{3/2}$ 5542.39	5d 26p 66310.48(5/2)
5	5	1646.992	60716.76	0.20	-0.005	29	10	$5d^26s (^3F)$	$^2F_{7/2}$ 17906.64	5d6s6p 78623.20(7/2)
68	9	1647.622	60693.52	-0.02	0.000	6	6	$5d^3$	$^2D_{3/2}$ 40470.77	5d6s6p 101164.31(1/2)
13	6	1651.943	60534.76	-0.21	0.006	23	18	$5d^3$	$^2D_{3/2}$ 12626.87	5d 26p 73161.84(5/2)
15	90	1652.720	60506.30	-0.02	0.001	22	15	$5d^3$	$^2G_{7/2}$ 11296.10	5d 26p 71802.42(7/2) Bl
200	90	1652.778	60504.18	0.20	-0.006	14	2	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	5d6s6p 79281.40(1/2) Bl
25	46	1658.906	60280.70	0.10	-0.003	32	12	$5d^3$	$^4P_{5/2}$ 14365.56	5d 26p 74646.16(3/2)
11	73	1660.657	60217.11	-0.02	0.000	14	13	$5d^26s (^3F)$	$^4F_{9/2}$ 13766.13	5d6s6p 73983.26(7/2)
316	81	1661.313	60193.35	-0.01	0.000	5	4	$5d^3$	$^2H_{11/2}$ 17553.75	5d 26p 77747.11(11/2)
60	90	1665.233	60051.66	0.10	-0.003	39	6	$5d^3$	$^2D_{5/2}$ 12134.38	5d 26p 72185.94(3/2)
9	81	1665.478	60042.82	-0.18	0.005	17	11	$5d^3$	$^2G_{9/2}$ 12350.26	5d 26p 72393.26(9/2)
49	81	1666.052	60022.15	0.11	-0.003	23	7	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	5d6s6p 78799.45(3/2)
52	19	1666.544	60004.41	-0.06	0.002	15	15	$5d^3$	$^2H_{9/2}$ 17800.85	5d 26p 77805.32(7/2)
71	73	1666.871	59992.63	0.02	-0.001	23	12	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	5d6s6p 78770.02(5/2)
84	73	1668.161	59946.26	0.00	0.000	15	4	$5d^3$	$^2H_{9/2}$ 17800.85	5d 26p 77747.11(11/2)
103	90	1669.485	59898.71	0.03	-0.001	29	15	$5d^26s (^3F)$	$^2F_{7/2}$ 17906.64	5d 26p 77805.32(7/2)
35	25	1672.123	59804.21	0.02	-0.001	19	14	$5d6s^2$	$^2D_{3/2}$ 28408.19	5d6s6p 88212.38(5/2)
134	90	1672.890	59776.80	0.01	0.000	16	4	$5d^3$	$^4F_{3/2}$ 0.0	5d 26p 59776.79(1/2)
9	38	1673.969	59738.25	-0.04	0.001	27	10	$5d^26s (^3F)$	$^4F_{7/2}$ 10425.17	5d6s6p 70163.46(5/2)
21	57	1675.940	59668.01	-0.03	0.001	39	15	$5d^3$	$^3D_{5/2}$ 12134.38	5d 26p 71802.42(7/2)
23	46	1676.131	59661.20	0.00	0.000	33	14	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	5d 26p 75381.05(7/2)
69	81	1679.560	59539.39	-0.01	0.000	18	15	$5d^3$	$^4F_{7/2}$ 4854.18	5d 26p 64393.59(7/2)
129	73	1680.014	59523.32	0.05	-0.001	39	13	$5d^3$	$^3D_{5/2}$ 12134.38	5d 26p 71657.65(3/2)
31	53	1680.709	59498.71	-0.27	0.008	26	9	$5d^3$	$^4P_{3/2}$ 15681.10	5d6s6p 75180.08(5/2)
55				0.42	-0.012	14	12	$5d^26s (^3P)$	$^2P_{3/2}$ 36499.67	5d6s6p 95997.96(5/2)
68	67	1681.541	59469.27	-0.18	0.005	26	4	$5d^3$	$^4P_{3/2}$ 15681.10	5d 26p 75150.55(1/2)
46				0.86	-0.024	23	9	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	5d 26p 78245.82(3/2)
20	40	1682.025	59452.15	-0.01	0.000	17	15	$5d^3$	$^2G_{9/2}$ 12350.26	5d 26p 71802.42(7/2)
24	16	1683.484	59400.63	-0.04	0.001	22	13	$5d^26s (^1D)$	$^2D_{3/2}$ 23796.27	5d6s6p 83196.94(5/2)
77	90	1685.741	59321.09	-0.35	0.010	27	15	$5d^26s (^3F)$	$^4F_{3/2}$ 5542.39	5d 26p 64863.83(3/2)
145	81	1689.029	59205.62	-0.15	0.004	15	15	$5d^3$	$^4F_{9/2}$ 6776.24	5d 26p 65982.01(7/2)
22	73	1689.209	59199.29	-0.09	0.003	18	17	$5d^3$	$^4F_{7/2}$ 4854.18	5d 26p 64053.56(5/2)
57	67	1690.876	59140.94	-0.15	0.004	28	8	$5d^3$	$^2P_{3/2}$ 7186.97	5d6s6p 66328.06(3/2)
84				-0.39	0.011	14	13	$5d^26s (^3P)$	$^2P_{3/2}$ 36499.67	5d6s6p 95641.00(3/2)
17	34	1691.377	59123.41	-0.10	0.003	28	13	$5d^3$	$^2P_{3/2}$ 7186.97	5d 26p 66310.48(5/2)
43	57	1694.032	59030.76	-0.02	0.001	23	13	$5d^3$	$^3D_{3/2}$ 12626.87	5d 26p 71657.65(3/2)
74	73	1694.084	59028.96	-0.06	0.002	29	17	$5d^26s (^3F)$	$^2F_{7/2}$ 17906.64	5d 26p 76935.66(5/2)
78	81	1694.555	59012.54	-0.13	0.004	27	16	$5d^26s (^3F)$	$^4F_{7/2}$ 10425.17	5d 26p 69437.84(7/2)
158	101	1694.762	59005.35	-0.04	0.001	28	13	$5d^26s (^3F)$	$^4F_{5/2}$ 7305.09	5d 26p 66310.48(5/2)
2	57	1695.723	58971.91	-0.07	0.002	27	12	$5d^26s (^3F)$	$^4F_{7/2}$ 10425.17	5d 26p 69397.15(5/2)
24	57	1695.920	58965.05	-0.01	0.000	26	12	$5d^3$	$^4P_{3/2}$ 15681.10	5d 26p 74646.16(3/2)
98	73	1697.035	58926.31	0.00	0.000	33	12	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	5d 26p 74646.16(3/2)
31	40	1699.621	58836.65	-0.26	0.007	18	14	$5d^3$	$^2F_{7/2}$ 29375.47	5d6s6p 88212.38(5/2)
26	67	1700.795	58796.05	-0.23	0.007	32	18	$5d^3$	$^4P_{5/2}$ 14365.56	5d 26p 73161.84(5/2)
128	61	1701.376	58775.96	-0.14	0.004	10	14	$5d^26s (^3P)$	$^2P_{1/2}$ 32953.36	5d 26p 91729.46(3/2)
46	73	1701.986	58754.89	-0.05	0.002	15	3	$5d^3$	$^4F_{9/2}$ 6776.24	5d 26p 65531.18(11/2)
1090	81	1703.539	58701.31	-0.14	0.004	4	10	$5d^3$	$^2D_{5/2}$ 42619.53	5d6s6p 101320.98(7/2)
131	90	1703.680	58696.45	-0.05	0.001	25	7	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	5d6s6p 78799.45(3/2)
5	6	1704.252	58676.78	-0.14	0.004	28	15	$5d^26s (^3F)$	$^4F_{5/2}$ 7305.09	5d 26p 65982.01(7/2)
327	90	1704.543	58666.74	-0.33	0.010	25	12	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	5d6s6p 78770.02(5/2)
81	67	1705.699	58626.99	-0.14	0.004	14	11	$5d^26s (^3F)$	$^4F_{9/2}$ 13766.13	5d 26p 72393.26(9/2)
242	101	1708.811	58520.22	-0.03	0.001	25	10	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	5d6s6p 78623.20(7/2)
18	157	1709.090	58510.66	-0.51	0.015	27	17	$5d^26s (^3F)$	$^4F_{3/2}$ 5542.39	5d 26p 64053.56(5/2) M TaV
3	32	1714.791	58316.13	0.00	0.000	16	9	$5d^3$	$^4F_{3/2}$ 0.0	5d 26p 58316.13(3/2)
19	101	1719.440	58158.46	0.22	-0.006	23	17	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	5d 26p 76935.66(5/2) M Al III
42	73	1719.936	58141.69	-0.05	0.002	22	16	$5d^3$	$^2G_{7/2}$ 11296.10	5d 26p 69437.84(7/2)
22	90	1721.141	58100.99	-0.06	0.002	22	12	$5d^3$	$^2G_{7/2}$ 11296.10	5d 26p 69397.15(5/2)
144	81	1721.731	58081.07	0.01	0.000	27	1			

Table I. Continued.

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark
454	90	1730.177	57797.54	-0.01	0.000	22	11	$5d^2 6s (^1D)$	$2D_{3/2}$ 23796.27	$5d^2 6p$ 81593.82(3/2)
687	73	1731.577	57750.82	0.02	-0.001	4	10	$5d^3$	$2D_{5/2}$ 42619.53	$5d^2 6p$ 100370.33(5/2)
309	115	1732.534	57718.91	0.00	0.000	15	7	$5d^3$	$2H_{9/2}$ 17800.85	$5d^2 6p$ 75519.76(9/2)
8	25	1732.769	57711.09	-0.15	0.004	27	10	$5d^2 6s (^3F)$	$4F_{7/2}$ 10425.17	$5d^2 6p$ 68136.41(9/2)
59	67	1733.032	57702.33	-0.04	0.001	25	15	$5d^2 6s (^3P)$	$4P_{5/2}$ 20102.95	$5d^2 6p$ 77805.32(7/2)
148	115	1733.664	57681.30	0.00	0.000	17	12	$5d^3$	$4F_{5/2}$ 2512.43	$5d^2 6p$ 60193.73(3/2)
27	81	1733.797	57676.89	0.03	-0.001	28	15	$5d^3$	$2P_{3/2}$ 7186.97	$5d^2 6p$ 64863.83(3/2)
66	90	1735.588	57617.36	0.01	0.000	15	15	$5d^3$	$4F_{9/2}$ 6776.24	$5d^2 6p$ 64393.59(7/2)
7	9	1735.653	57615.21	-0.01	0.000	14	12	$5d^2 6s (^3P)$	$4P_{1/2}$ 17030.94	$5d^2 6p$ 74646.16(3/2)
15	67	1735.922	57606.29	0.03	-0.001	16	11	$5d^3$	$4F_{3/2}$ 0.0	$5d^2 6p$ 57606.26(5/2)
301	133	1736.437	57589.19	0.14	-0.004	18	14	$5d^3$	$4F_{7/2}$ 4854.18	$5d^2 6p$ 62443.23(5/2)
396	101	1736.709	57580.18	-0.02	0.001	15	14	$5d^3$	$2H_{9/2}$ 17800.85	$5d^2 6p$ 75381.05(7/2)
16	81	1737.047	57568.95	-0.02	0.001	17	13	$5d^3$	$4F_{5/2}$ 2512.43	$5d^2 6p$ 60081.40(7/2)
20	53	1737.354	57558.80	0.06	-0.002	28	15	$5d^2 6s (^3F)$	$4F_{5/2}$ 7305.09	$5d^2 6p$ 64863.83(3/2)
226	53	1739.907	57474.34	-0.07	0.002	29	14	$5d^2 6s (^3F)$	$2F_{7/2}$ 17906.64	$5d^2 6p$ 75381.05(7/2)
4	3	1741.043	57436.83	-0.03	0.001	32	15	$5d^3$	$4P_{5/2}$ 14365.56	$5d^2 6p$ 71802.42(7/2)
234	67	1741.692	57415.43	0.01	0.000	24	13	$5d^2 6s (^1D)$	$2D_{5/2}$ 25781.52	$5d^6s6p$ 83196.94(5/2)
69	61	1745.096	57303.45	-0.01	0.000	39	16	$5d^3$	$2D_{5/2}$ 12134.38	$5d^2 6p$ 69437.84(7/2)
66	73	1745.437	57292.26	0.17	-0.005	32	13	$5d^3$	$4P_{5/2}$ 14365.56	$5d^2 6p$ 71657.65(3/2)
42	57	1746.010	57273.43	-0.01	0.000	29	9	$5d^2 6s (^3F)$	$2F_{7/2}$ 17906.64	$5d^6s6p$ 75180.08(5/2)
5	61	1746.335	57262.80	0.03	-0.001	39	12	$5d^3$	$2D_{5/2}$ 12134.38	$5d^2 6p$ 69397.15(5/2)
256	81	1747.942	57210.13	0.00	0.000	22	14	$5d^3$	$2G_{7/2}$ 11296.10	$5d^2 6p$ 68506.23(5/2)
543	101	1751.695	57087.55	-0.03	0.001	17	16	$5d^3$	$2G_{9/2}$ 12350.26	$5d^2 6p$ 69437.84(7/2)
11	22	1754.972	56980.96	-0.01	0.001	13	15	$5d^3$	$2P_{1/2}$ 7882.85	$5d^2 6p$ 64863.83(3/2)
44	73	1757.446	56900.75	-0.09	0.003	27	14	$5d^2 6s (^3F)$	$4F_{3/2}$ 5542.39	$5d^2 6p$ 62443.23(5/2)
58	73	1757.837	56888.09	-0.02	0.001	18	11	$5d^3$	$4F_{7/2}$ 4854.18	$5d^2 6p$ 61742.29(7/2)
91	90	1758.038	56881.59	-0.06	0.002	26	6	$5d^3$	$4P_{3/2}$ 15681.10	$5d^2 6p$ 72562.75(1/2) TaIV
13				0.31	-0.010	27	9	$5d^2 6s (^3F)$	$4F_{3/2}$ 5542.39	$5d^2 6p$ 62423.67(1/2)
7	46	1758.502	56866.58	-0.01	0.000	28	17	$5d^3$	$2P_{3/2}$ 7186.97	$5d^2 6p$ 64053.56(5/2)
5	4	1759.314	56840.33	0.02	-0.001	22	10	$5d^3$	$2G_{7/2}$ 11296.10	$5d^2 6p$ 68136.41(9/2)
82	81	1759.549	56832.75	0.04	-0.001	25	17	$5d^2 6s (^3P)$	$4P_{5/2}$ 20102.95	$5d^2 6p$ 76935.66(5/2)
42	26	1763.287	56712.27	0.00	0.000	10	4	$5d^3$	$4P_{1/2}$ 12805.56	$5d^6s6p$ 69517.83(1/2)
34	61	1766.886	56596.75	0.02	-0.001	39	15	$5d^3$	$2D_{5/2}$ 12134.38	$5d^2 6p$ 68731.11(3/2)
382	115	1767.946	56562.83	0.01	0.000	15	10	$5d^3$	$4F_{9/2}$ 6776.24	$5d^2 6p$ 63339.06(9/2)
337	90	1772.966	56402.68	0.01	0.000	23	9	$5d^2 6s (^3P)$	$4P_{3/2}$ 18777.41	$5d^6s6p$ 75180.08(5/2)
8	2	1773.934	56371.88	0.03	-0.001	39	14	$5d^3$	$2D_{5/2}$ 12134.38	$5d^2 6p$ 68506.23(5/2)
7	1	1774.866	56342.29	-0.01	0.001	24	13	$5d^3$	$2F_{5/2}$ 26854.64	$5d^6s6p$ 83196.94(5/2)
56	53	1777.632	56254.61	0.00	0.000	19	10	$5d^6s^2$	$2D_{3/2}$ 28408.19	$5d^2 6p$ 84662.80(1/2)
141	73	1778.548	56225.65	-0.05	0.002	19	13	$5d^2 6s (^1G)$	$2G_{7/2}$ 26971.24	$5d^6s6p$ 83196.94(5/2)
9	67	1779.922	56182.24	-0.17	0.006	15	13	$5d^3$	$2H_{9/2}$ 17800.85	$5d^6s6p$ 73983.26(7/2)
19	57	1780.440	56165.89	-0.10	0.003	28	14	$5d^3$	$2P_{3/2}$ 7186.97	$5d^2 6p$ 63352.96(3/2)
25	30	1780.991	56148.50	-0.07	0.002	18	14	$5d^6s^2$	$2D_{5/2}$ 32063.81	$5d^6s6p$ 88212.38(5/2)
63	90	1781.539	56131.24	-0.03	0.001	23	8	$5d^3$	$2D_{3/2}$ 12626.87	$5d^2 6p$ 68758.14(1/2)
33	53	1783.086	56082.54	-0.03	0.001	33	15	$5d^2 6s (^3F)$	$2F_{5/2}$ 15719.85	$5d^2 6p$ 71802.42(7/2)
9	49	1783.268	56076.82	0.20	-0.006	29	13	$5d^2 6s (^3F)$	$2F_{7/2}$ 17906.64	$5d^6s6p$ 73983.26(7/2)
32	67	1784.190	56047.85	-0.02	0.001	28	14	$5d^2 6s (^3F)$	$4F_{5/2}$ 7305.09	$5d^2 6p$ 63352.96(3/2)
75	67	1786.464	55976.50	-0.05	0.002	26	13	$5d^3$	$4P_{3/2}$ 15681.10	$5d^2 6p$ 71657.65(3/2)
14	61	1787.229	55952.54	-0.05	0.001	10	8	$5d^3$	$4P_{1/2}$ 12805.56	$5d^2 6p$ 68758.14(1/2)
72	81	1787.700	55937.81	0.01	0.000	33	13	$5d^2 6s (^3F)$	$2F_{5/2}$ 15719.85	$5d^2 6p$ 71657.65(3/2)
21	46	1788.092	55925.53	-0.02	0.001	10	15	$5d^3$	$4P_{1/2}$ 12805.56	$5d^2 6p$ 68731.11(3/2)
44	73	1789.378	55885.34	0.03	-0.001	27	13	$5d^2 6s (^3F)$	$4F_{7/2}$ 10425.17	$5d^2 6p$ 66310.48(5/2)
22	61	1789.570	55879.36	0.00	0.000	23	14	$5d^3$	$2D_{3/2}$ 12626.87	$5d^2 6p$ 68506.23(5/2)
42	40	1789.912	55868.68	-0.07	0.002	23	12	$5d^2 6s (^3P)$	$4P_{3/2}$ 18777.41	$5d^2 6p$ 74646.16(3/2)
8	57	1792.007	55803.34	-0.36	0.012	17	9	$5d^3$	$4F_{5/2}$ 2512.43	$5d^2 6p$ 58316.13(3/2)
2	1	1792.186	55797.77	-0.13	0.004	32	10	$5d^3$	$4P_{5/2}$ 14365.56	$5d^6s6p$ 70163.46(5/2)
220	90	1792.554	55786.32	0.17	-0.006	17	10	$5d^3$	$2G_{9/2}$ 12350.26	$5d^2 6p$ 68136.41(9/2)
39				-0.74	0.024	22	13	$5d^2 6s (^1D)$	$2D_{3/2}$ 23796.27	$5d^2 6p$ 79583.33(5/2)
40	61	1799.955	55556.93	0.09	-0.003	27	15	$5d^2 6s (^3F)$	$4F_{7/2}$ 10425.17	$5d^2 6p$ 65982.01(7/2)
32	34	1800.749	55532.45	0.64	-0.021	14	6	$5d^2 6s (^3P)$	$4P_{1/2}$ 17030.94	$5d^2 6p$ 72562.75(1/2) Hfs
40	40	1800.781	55531.47	-0.34	0.011					Hfs
423	61	1800.920	55527.16	-0.03	0.001	6	12	$5d^3$	$2D_{3/2}$ 40470.77	$5d^6s6p$ 95997.96(5/2)
11	43	1805.403	55389.28	0.13	-0.004	16	13	$5d^3$	$4F_{3/2}$ 0.0	$5d^2 6p$ 55389.15(5/2)
50	67	1806.418	55358.18	0.07	-0.002	23	12	$5d^3$	$2D_{3/2}$ 12626.87	$5d^2 6p$ 67984.98(3/2)
31	67	1809.031	55278.23	0.13	-0.004	25	14	$5d^2 6s (^3P)$	$4P_{5/2}$ 20102.95	$5d^2 6p$ 75381.05(7/2)
16	20	1809.750	55256.25	-0.01	0.000	28	14	$5d^3$	$2P_{3/2}$ 7186.97	$5d^2 6p$ 62443.23(5/2)
19	40	1809.785	55255.18	-0.02	0.001	29	18	$5d^2 6s (^3F)$	$2F_{7/2}$ 17906.64	$5d^2 6p$ 73161.84(5/2)
28	67	1810.390	55236.72	0.02	-0.001	28	9	$5d^3$	$2P_{3/2}$ 7186.97	$5d^2 6p$ 62423.67(1/2)
28	49	1810.614	55229.88	0.09	-0.003	14	14	$5d^2 6s (^3P)$	$2P_{3/2}$ 36499.67	$5d^2 6p$ 91729.46(3/2)
259	115	1810.695	55227.42	0.20	-0.007	18	13	$5d^3$	$4F_{7/2}$ 4854.18	$5d^2 6p$ 60081.40(7/2)
56	57	1812.268	55179.48	0.06	-0.002	10	12	$5d^3$	$4P_{1/2}$ 12805.56	$5d^2 6p$ 67984.98(3/2)
230	49	1812.570	55170.29	0.06	-0.002	6	13	$5d^3$	$2D_{3/2}$ 40470.77	$5d^6s6p$ 95641.00(3/2)
267	90	1813.069	55155.10	0.10	-0.003	14	6	$5d^2 6s (^3P)$	$4P_{1/2}$ 17030.94	$5d^2 6p$ 72185.94(3/2)
201	101	1813.624	55138.22							

Table I. *Continued.*

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level		Odd level	Remark	
16	1	1824.726	54802.75	0.22	-0.007	14	4	$5d^26s$ (3P)	$^2P_{3/2}$	36499.67	$5d^26p$	91302.20(1/2)
15	1	1825.178	54789.17	0.42	-0.014	19	13	$5d6s^2$	$^2D_{3/2}$	28408.19	$5d6s6p$	83196.94(5/2)
32	12	1826.843	54739.24	0.06	-0.002	24	11	$5d^3$	$^2F_{5/2}$	26854.64	$5d^26p$	81593.82(3/2)
250	81	1828.620	54686.04	0.13	-0.004	22	15	$5d^3$	$^2G_{7/2}$	11296.10	$5d^26p$	65982.01(7/2)
232	90	1829.776	54651.48	0.14	-0.005	27	12	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39	$5d^26p$	60193.73(3/2)
135	73	1831.759	54592.34	-0.07	0.002	15	11	$5d^3$	$^2H_{9/2}$	17800.85	$5d^26p$	72393.26(9/2)
38	61	1833.489	54540.82	0.00	0.000	13	9	$5d^3$	$^2P_{1/2}$	7882.85	$5d^26p$	62423.67(1/2)
182	90	1835.314	54486.58	-0.04	0.002	29	11	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64	$5d^26p$	72393.26(9/2)
26	81	1835.452	54482.50	0.14	-0.005	26	10	$5d^3$	$^4P_{3/2}$	15681.10	$5d6s6p$	70163.46(5/2)
241	90	1836.978	54437.24	0.04	-0.001	28	11	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09	$5d^26p$	61742.29(7/2)
42	38	1838.761	54384.46	0.03	-0.001	23	18	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41	$5d^26p$	73161.84(5/2)
393	101	1839.237	54370.38	0.10	-0.004	14	10	$5d^26s$ (3F)	$^4F_{9/2}$	13766.13	$5d^26p$	68136.41(9/2)
43	90	1843.850	54234.34	-0.06	0.002	27	4	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39	$5d^26p$	59776.79(1/2)
60	67	1845.235	54193.63	-0.05	0.002	39	8	$5d^3$	$^2D_{5/2}$	12134.38	$5d6s6p$	66328.06(3/2)
62	81	1845.830	54176.16	0.06	-0.002	39	13	$5d^3$	$^2D_{5/2}$	12134.38	$5d^26p$	66310.48(5/2)
74	73	1847.041	54140.65	-0.02	0.001	32	14	$5d^3$	$^4P_{5/2}$	14365.56	$5d^26p$	68506.23(5/2)
69	80	1850.008	54053.81	0.05	-0.002	18	8	$5d^3$	$^4F_{7/2}$	4854.18	$5d^26p$	58907.94(9/2)
133	85	1851.795	54001.64	0.08	-0.003	15	15	$5d^3$	$^2H_{9/2}$	17800.85	$5d^26p$	71802.42(7/2)
161	105	1855.426	53895.97	0.19	-0.006	29	15	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64	$5d^26p$	71802.42(7/2)
126	105	1855.938	53881.11	0.80	-0.028	25	13	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95	$5d6s6p$	73983.26(7/2)
16	71	1857.090	53847.70	0.06	-0.002	39	15	$5d^3$	$^2D_{5/2}$	12134.38	$5d^26p$	65982.01(7/2)
12	1	1858.666	53802.02	0.21	-0.007	24	13	$5d^26s$ (1D)	$^2D_{5/2}$	25781.52	$5d^26p$	79583.33(5/2)
40	67	1859.238	53785.48	0.14	-0.005	23	6	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41	$5d^26p$	72562.75(1/2)
88	98	1859.739	53771.00	0.07	-0.002	28	5	$5d^3$	$^2P_{3/2}$	7186.97	$5d^26p$	60957.90(1/2)
25	49	1861.571	53718.08	0.09	-0.003	33	16	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85	$5d^26p$	69437.84(7/2)
63	47	1861.636	53716.19	0.14	-0.005	26	12	$5d^3$	$^4P_{3/2}$	15681.10	$5d^26p$	69397.15(5/2)
10	34	1862.158	53701.15	-0.04	0.001	23	8	$5d^3$	$^2D_{3/2}$	12626.87	$5d6s6p$	66328.06(3/2)
4	85	1862.993	53677.07	-0.23	0.008	33	12	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85	$5d^26p$	69397.15(5/2)
43	85	1864.565	53631.82	0.07	-0.002	17	15	$5d^3$	$^2G_{9/2}$	12350.26	$5d^26p$	65982.01(7/2)
12	16	1864.679	53628.53	0.14	-0.005	27	17	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17	$5d^26p$	64053.56(5/2)
36	80	1864.998	53619.36	-0.06	0.002	32	12	$5d^3$	$^4P_{5/2}$	14365.56	$5d^26p$	67984.98(3/2)
39	75	1868.373	53522.51	0.01	0.000	10	8	$5d^3$	$^4P_{1/2}$	12805.56	$5d6s6p$	66328.06(3/2)
172	91	1880.371	53180.99	0.07	-0.002	17	3	$5d^3$	$^2G_{9/2}$	12350.26	$5d^26p$	65531.18(11/2)
15	7	1881.843	53139.40	0.01	0.000	22	17	$5d^26s$ (1D)	$^2D_{3/2}$	23796.27	$5d^26p$	76935.66(5/2)
202	105	1883.327	53097.52	0.03	-0.001	22	15	$5d^3$	$^2G_{7/2}$	11296.10	$5d^26p$	64393.59(7/2)
14	37	1884.054	53077.03	-0.01	0.000	26	8	$5d^3$	$^4P_{3/2}$	15681.10	$5d^26p$	68758.14(1/2)
30	1	1884.700	53058.84	-0.05	0.002	25	18	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95	$5d^26p$	73161.84(5/2)
13	6	1885.015	53049.99	-0.02	0.001	26	15	$5d^3$	$^4P_{3/2}$	15681.10	$5d^26p$	68731.11(3/2)
16	23	1886.391	53011.27	0.01	0.000	33	15	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85	$5d^26p$	68731.11(3/2)
7	4	1886.554	53006.70	-0.06	0.002	28	12	$5d^3$	$^2P_{3/2}$	7186.97	$5d^26p$	60193.73(3/2)
168	75	1887.206	52988.40	-0.10	0.004	24	12	$5d^26s$ (1D)	$^2D_{5/2}$	25781.52	$5d6s6p$	78770.02(5/2)
499	113	1889.864	52913.87	-0.02	0.001	27	10	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17	$5d^26p$	63339.06(9/2)
31	75	1890.765	52888.66	0.02	-0.001	28	12	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09	$5d^26p$	60193.73(3/2)
22	41	1891.071	52880.10	-0.14	0.005	23	13	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41	$5d^26p$	71657.65(3/2)
85	105	1891.197	52876.57	-0.15	0.005	17	13	$5d^3$	$^4F_{5/2}$	2512.43	$5d^26p$	55389.15(5/2)
43	7	1892.447	52841.64	-0.04	0.002	24	10	$5d^26s$ (1D)	$^2D_{5/2}$	25781.52	$5d6s6p$	78623.20(7/2)
28	57	1893.041	52825.05	-0.08	0.003	26	14	$5d^3$	$^4P_{3/2}$	15681.10	$5d^26p$	68506.23(5/2)
109	105	1894.429	52786.36	-0.03	0.001	33	14	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85	$5d^26p$	68506.23(5/2)
107	147	1894.792	52776.24	-0.07	0.002	28	13	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09	$5d^26p$	60081.40(7/2)
73	134	1894.880	52773.80	0.06	-0.002	27	9	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39	$5d^26p$	58316.13(3/2)
49	85	1895.469	52757.39	-0.07	0.003	22	17	$5d^3$	$^2G_{7/2}$	11296.10	$5d^26p$	64053.56(5/2)
6	34	1895.665	52751.95	-0.14	0.005	18	11	$5d^3$	$^4F_{7/2}$	4854.18	$5d^26p$	57606.26(5/2)
7	1	1896.377	52732.13	-0.10	0.004	13	7	$5d^26s$ (1G)	$^2G_{9/2}$	27329.62	$5d6s6p$	80061.85(9/2)
2	1	1896.475	52729.39	-0.05	0.002	39	15	$5d^3$	$^2D_{5/2}$	12134.38	$5d^26p$	64863.83(3/2)
147	80	1900.703	52612.10	0.01	0.000	19	13	$5d^26s$ (1G)	$^2G_{7/2}$	26971.24	$5d^26p$	79583.33(5/2)
15	45	1905.243	52486.73	-0.16	0.006	14	4	$5d^26s$ (3P)	$^4P_{1/2}$	17030.94	$5d6s6p$	69517.83(1/2)
41	57	1906.059	52464.28	-0.02	0.001	24	9	$5d^26s$ (1D)	$^2D_{5/2}$	25781.52	$5d^26p$	78245.82(3/2)
129	4	1909.813	52361.16	-0.01	0.001	4	13	$5d^26s$ (1S)	$^2S_{1/2}$	43279.83	$5d6s6p$	95641.00(3/2)
129	1	1909.886	52359.14	0.13	-0.005	4	13	$5d^26s$ (1S)	$^2S_{1/2}$	43281.99	$5d6s6p$	95641.00(3/2)
9	37	1911.649	52310.85	-0.03	0.001	13	12	$5d^3$	$^2P_{1/2}$	7882.85	$5d^26p$	60193.73(3/2)
16	45	1911.904	52303.88	0.00	0.000	26	12	$5d^3$	$^4P_{3/2}$	15681.10	$5d^26p$	67984.98(3/2)
12	1	1913.326	52265.01	-0.12	0.004	33	12	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85	$5d^26p$	67984.98(3/2)
183	105	1913.544	52259.07	-0.14	0.005	39	15	$5d^3$	$^3D_{5/2}$	12134.38	$5d^26p$	64393.59(7/2)
49	85	1913.624	52256.88	0.06	-0.002	29	10	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64	$5d6s6p$	70163.46(5/2)
28	47	1914.355	52236.91	-0.05	0.002	23	15	$5d^3$	$^3D_{3/2}$	12626.87	$5d^26p$	64863.83(3/2)
20	41	1915.128	52215.82	-0.06	0.002	14	15	$5d^26s$ (3F)	$^4F_{9/2}$	13766.13	$5d^26p$	65982.01(7/2)
142	113	1915.568	52203.84	-0.08	0.003	16	9	$5d^3$	$^4F_{3/2}$	0.0	$5d^26p$	52203.92(3/2)
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Table I. Continued.

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark
18	1	1933.876	51709.62	0.18	-0.007	10	10	$5d^26s$ (3P)	$^2P_{1/2}$	32953.36
208	91	1934.250	51699.62	0.15	-0.006	25	15	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95
66	71	1936.594	51637.05	0.06	-0.002	15	16	$5d^3$	$^2H_{9/2}$	17800.85
26	60	1937.365	51616.50	0.05	-0.002	32	15	$5d^3$	$^4P_{5/2}$	14365.56
39	1	1939.680	51554.90	0.20	-0.007	25	13	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95
93	91	1940.566	51531.35	0.15	-0.006	29	16	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64
62	91	1944.094	51437.83	0.10	-0.004	17	11	$5d^3$	$^4F_{5/2}$	2512.43
69	80	1944.511	51426.80	0.12	-0.004	23	17	$5d^3$	$^3D_{3/2}$	12626.87
19	1	1945.860	51391.17	-0.01	0.000	24	9	$5d^3$	$^2F_{5/2}$	26854.64
1	16	1946.056	51385.99	-0.06	0.002	23	10	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41
17	5	1946.138	51383.82	0.01	0.000	22	9	$5d^26s$ (1D)	$^2D_{3/2}$	23796.27
92	105	1948.669	51317.07	-0.05	0.002	27	11	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
63	51	1949.562	51293.56	-0.02	0.001	13	10	$5d^26s$ (1G)	$^2G_{9/2}$	27329.62
70	113	1952.415	51218.63	0.05	-0.002	39	14	$5d^3$	$^3D_{5/2}$	12134.38
132	147	1954.064	51175.39	0.25	-0.010	19	13	$5d6s^2$	$^2D_{3/2}$	28408.19
49	105	1955.147	51147.05	-0.08	0.003	22	14	$5d^3$	$^2G_{7/2}$	11296.10
11	162	1955.687	51132.93	-0.20	0.008	18	13	$5d6s^2$	$^2D_{5/2}$	32063.81
40	105	1961.216	50988.77	-0.03	0.001	17	10	$5d^3$	$^2G_{9/2}$	12350.26
9	7	1962.532	50954.58	0.54	-0.021	14	12	$5d^26s$ (3P)	$^4P_{1/2}$	17030.94
9		1962.583	50953.27	-0.77	0.030					Hfs
28	60	1962.683	50950.65	-0.03	0.001	24	15	$5d^3$	$^2F_{5/2}$	26854.64
50	18	1967.187	50834.02	-0.06	0.002	19	15	$5d^26s$ (1G)	$^2G_{7/2}$	26971.24
27	98	1971.373	50726.08	-0.01	0.000	23	14	$5d^3$	$^3D_{3/2}$	12626.87
33	40	1975.138	50629.37	-0.01	0.000	26	13	$5d^3$	$^4P_{3/2}$	15681.10
116	180	1975.212	50627.48	0.02	-0.001	14	15	$5d^26s$ (3F)	$^4F_{9/2}$	13766.13
85	123	1975.516	50619.70	-0.04	0.002	23	12	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41
8	1	1976.302	50599.57	-0.02	0.001	29	14	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64
18	71	1978.343	50547.34	-0.06	0.002	10	14	$5d^3$	$^4P_{1/2}$	12805.56
5	2	1980.271	50498.15	-0.12	0.005	32	15	$5d^3$	$^4P_{5/2}$	14365.56
114	105	1981.155	50475.60	-0.10	0.004	13	15	$5d^26s$ (1G)	$^2G_{9/2}$	27329.62
82	162	1982.821	50433.19	-0.09	0.004	13	9	$5d^3$	$^2P_{1/2}$	7882.85
86	150	1983.368	50419.29	0.00	0.000	28	11	$5d^3$	$^2P_{3/2}$	7186.97
913	230	1983.439	50417.48	-0.01	0.000	13	4	$5d^26s$ (1G)	$^2G_{9/2}$	27329.62
39	123	1986.671	50335.46	-0.10	0.004	15	10	$5d^3$	$^2H_{9/2}$	17800.85
62	147	1988.033	50300.96	-0.20	0.008	28	11	$5d^26s$ (3F)	$^4F_{5/2}$	7305.09
235	230	1989.572	50262.08	-0.08	0.003	33	15	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85
112	162	1990.854	50229.70	-0.07	0.003	29	10	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64
78	98	1991.722	50207.80	-0.05	0.002	18	13	$5d^3$	$^2F_{7/2}$	29375.47
23	14	1996.769	50080.91	-0.11	0.004	24	17	$5d^3$	$^2F_{5/2}$	26854.64
43	123	1997.586	50060.42	-0.09	0.004	25	10	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95
154	147	1998.882	50027.96	-0.07	0.003	32	15	$5d^3$	$^4P_{5/2}$	14365.56
4	1	2000.120	49980.80	0.07	-0.003	23	8	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41
63	85	2000.777	49964.39	-0.03	0.001	19	17	$5d^26s$ (1G)	$^2G_{7/2}$	26971.24
35	71	2001.206	49953.70	0.00	0.000	23	15	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41
5	1	2005.502	49846.70	-0.06	0.002	27	13	$5d^26s$ (3F)	$^4F_{3/2}$	5542.39
30	75	2005.861	49837.79	0.16	-0.006	19	9	$5d6s^2$	$^2D_{3/2}$	28408.19
70	134	2006.724	49816.34	-0.02	0.001	23	14	$5d^3$	$^3D_{3/2}$	12626.87
97	180	2013.192	49656.32	0.09	-0.004	27	13	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
50	123	2015.156	49607.93	0.02	-0.001	39	11	$5d^3$	$^3D_{5/2}$	12134.38
126	113	2015.498	49599.52	-0.01	0.000	24	14	$5d^26s$ (1D)	$^2D_{5/2}$	25781.52
96	162	2016.579	49572.92	-0.01	0.000	14	10	$5d^26s$ (3F)	$^4F_{9/2}$	13766.13
36	9	2018.326	49530.04	0.03	-0.001	18	11	$5d6s^2$	$^2D_{5/2}$	32063.81
22	75	2023.965	49392.05	0.02	-0.001	17	11	$5d^3$	$^2G_{9/2}$	12350.26
13	2	2025.052	49365.55	-0.02	0.001	22	18	$5d^26s$ (1D)	$^2D_{3/2}$	23796.27
8	16	2027.842	49297.64	0.52	-0.021	14	8	26s (3P)	$^4P_{1/2}$	17030.94
30		2027.889	49296.49	-0.63	0.026					Hfs
56	27	2027.983	49294.21	0.01	0.000	25	12	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95
35	1	2029.892	49247.86	0.13	-0.005	18	10	$5d^3$	$^2F_{7/2}$	29375.47
14	51	2031.555	49207.54	-0.04	0.001	23	12	$5d^26s$ (3P)	$^4P_{3/2}$	18777.41
8	10	2032.582	49182.70	-0.04	0.001	26	15	$5d^3$	$^4P_{3/2}$	15681.10
23	63	2034.183	49143.99	0.01	0.000	33	15	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85
81	18	2035.591	49110.00	0.07	-0.003	4	14	$5d^3$	$^2D_{5/2}$	42619.53
4	14	2036.174	49095.94	-0.04	0.002	18	11	$5d^3$	$^4F_{7/2}$	4854.18
16	8	2049.936	48766.38	-0.10	0.004	22	6	$5d^26s$ (1D)	$^2D_{3/2}$	23796.27
21	60	2053.836	48673.80	0.06	-0.003	33	15	$5d^26s$ (3F)	$^2F_{5/2}$	15719.85
37	8	2055.245	48640.42	-0.04	0.002	10	11	$5d^26s$ (3P)	$^2P_{1/2}$	32953.36
29	134	2055.782	48627.71	-0.45	0.019	25	15	$5d^26s$ (3P)	$^4P_{5/2}$	20102.95
411	91	2059.131	48548.64	0.13	-0.005	19	7	$5d^26s$ (1G)	$^2G_{7/2}$	26971.24
42	47	2060.030	48527.47	0.00	0.000	19	17	$5d^26s^2$	$^2D_{3/2}$	28408.19
39	29	2060.075	48526.41	0.00	0.000	24	14	$5d^3$	$^2F_{5/2}$	26854.64
244	105	2061.930	48482.76	-0.01	0.001	27	8	$5d^26s$ (3F)	$^4F_{7/2}$	10425.17
123	19	2063.336	48449.73	0.10	-0.004	4	14	$5d^26s$ (1S)	$^2S_{1/2}$	43279.83
123	29	2063.433	48447.43	-0.04	0.002	4	14	$5d^26s$ (1S)	$^2S_{1/2}$	43281.99
113	63	2064.183	48429.84	-0.01	0.000	18	15	$5d^3$	$^2F_{7/2}$	29375.47
35	13	2065.037	48409.81	0.00	0.000	19	14	$5d^26s$ (1G)	$^2G_{7/2}$	26971.24
89	91	2065.292	48403.84	0.00	0.000	29	13	$5d^26s$ (3F)	$^2F_{7/2}$	17906.64
42	71	2066.632	48372.46	0.00	0.000	26	17	$5d^3$	$^4P_{3/2}$	15681.10
										Hfs
										M TaIV
										F = 3
										F = 4

Table I. *Continued.*

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm $^{-1}$)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level		Odd level	Remark	
121	91	2068.285	48333.79	0.08	-0.004	33	17	5d ² 6s (³ F)	² F _{5/2}	15719.85	5d ² 6p	64053.56(5/2)
6	7	2068.405	48331.00	-0.03	0.002	23	5	5d ³	³ D _{3/2}	12626.87	5d ² 6p	60957.90(1/2)
98	105	2073.941	48202.01	-0.17	0.007	28	13	5d ³	² P _{3/2}	7186.97	5d ² 6p	55389.15(5/2)
11				0.27	-0.012	24	13	5d ² 6s (¹ D)	² D _{5/2}	25781.52	5d6s6p	73983.26(7/2)
49	105	2074.121	48197.82	-0.03	0.002	16	7	5d ³	⁴ F _{3/2}	0.0	5d ² 6p	48197.85(5/2)
200	91	2074.454	48190.08	-0.06	0.003	13	7	5d ² 6s (¹ G)	² G _{9/2}	27329.62	5d ² 6p	75519.76(9/2)
21	1	2075.613	48163.17	0.04	-0.002	14	10	5d ² 6s (³ P)	² P _{3/2}	36499.67	5d ² 6p	84662.80(1/2)
16	49	2076.085	48152.22	-0.12	0.005	10	5	5d ³	⁴ P _{1/2}	12805.56	5d ² 6p	60957.90(1/2)
24	80	2079.029	48084.06	0.00	0.000	28	13	5d ² 6s (³ F)	⁴ F _{5/2}	7305.09	5d ² 6p	55389.15(5/2)
19	63	2079.313	48077.48	-0.19	0.009	32	14	5d ³	⁴ P _{5/2}	14365.56	5d ² 6p	62443.23(5/2)
11	49	2079.407	48075.30	-0.06	0.003	29	15	5d ² 6s (³ F)	² F _{7/2}	17906.64	5d ² 6p	65982.01(7/2)
46	75	2080.098	48059.35	0.00	0.000	39	12	5d ³	³ D _{5/2}	12134.38	5d ² 6p	60193.73(3/2)
124	13	2081.700	48022.37	0.00	0.000	4	4	5d ² 6s (¹ S)	² S _{1/2}	43279.83	5d ² 6p	91302.20(1/2)
124	24	2081.792	48020.23	0.02	-0.001	4	4	5d ² 6s (¹ S)	² S _{1/2}	43281.99	5d ² 6p	91302.20(1/2)
62	85	2083.707	47976.13	-0.04	0.001	14	11	5d ² 6s (³ F)	⁴ F _{9/2}	13766.13	5d ² 6p	61742.29(7/2)
53	75	2084.974	47946.96	-0.06	0.003	39	13	5d ³	³ D _{5/2}	12134.38	5d ² 6p	60081.40(7/2)
95	75	2087.806	47881.93	-0.10	0.005	25	12	5d ² 6s (³ P)	⁴ P _{5/2}	20102.95	5d ² 6p	67984.98(3/2)
21	45	2088.701	47861.42	0.04	-0.002	22	13	5d ² 6s (¹ D)	² D _{3/2}	23796.27	5d ² 6p	71657.65(3/2)
120	80	2091.758	47791.48	-0.04	0.002	24	12	5d ³	² F _{5/2}	26854.64	5d ² 6p	74646.16(3/2)
25	63	2094.407	47731.04	-0.10	0.005	17	13	5d ³	² G _{9/2}	12350.26	5d ² 6p	60081.40(7/2)
4	1	2097.004	47671.94	0.08	-0.004	26	14	5d ³	⁴ P _{3/2}	15681.10	5d ² 6p	63352.96(3/2)
18	41	2098.713	47633.12	0.01	-0.001	33	14	5d ² 6s (³ F)	² F _{5/2}	15719.85	5d ² 6p	63352.96(3/2)
19	54	2099.657	47611.71	-0.13	0.006	22	8	5d ³	² G _{7/2}	11296.10	5d ² 6p	58907.94(9/2)
5	1	2101.641	47566.77	-0.09	0.004	23	12	5d ³	³ D _{3/2}	12626.87	5d ² 6p	60193.73(3/2)
42	43	2101.935	47560.11	-0.08	0.003	18	17	5d ³	² F _{7/2}	29375.47	5d ² 6p	76935.66(5/2)
28	37	2103.133	47533.03	-0.04	0.002	23	13	5d ² 6s (³ P)	⁴ P _{3/2}	18777.41	5d ² 6p	66310.48(5/2)
106	71	2103.728	47519.58	0.06	-0.003	18	13	5d6s ²	² D _{5/2}	32063.81	5d ² 6p	79583.33(5/2)
37	51	2109.917	47380.22	-0.10	0.005	24	18	5d ² 6s (¹ D)	² D _{5/2}	25781.52	5d ² 6p	73161.84(5/2)
34	63	2110.079	47376.57	-0.16	0.007	32	11	5d ³	⁴ P _{5/2}	14365.56	5d ² 6p	61742.29(7/2)
41	80	2118.822	47181.11	0.01	-0.001	27	11	5d ² 6s (³ F)	⁴ F _{7/2}	10425.17	5d ² 6p	57606.26(5/2)
8	13	2119.144	47173.95	0.03	-0.001	15	11	5d ³	⁴ F _{9/2}	6776.24	5d ² 6p	53950.16(7/2)
7	3	2126.443	47012.03	0.01	0.000	19	13	5d ² 6s (¹ G)	² G _{7/2}	26971.24	5d6s6p	73983.26(7/2)
21	57	2138.705	46742.52	0.16	-0.008	19	4	5d6s ²	² D _{3/2}	28408.19	5d ² 6p	75150.55(1/2)
8				-0.05	0.002	26	9	5d ³	⁴ P _{3/2}	15681.10	5d ² 6p	62423.67(1/2)
20	4	2139.574	46723.54	0.16	-0.007	33	14	5d ² 6s (³ F)	² F _{5/2}	15719.85	5d ² 6p	62443.23(5/2)
21	98	2142.414	46661.61	0.08	-0.004	27	9	5d ² 6s (³ F)	⁴ F _{3/2}	5542.39	5d ² 6p	52203.92(3/2)
233	180	2143.171	46645.13	0.06	-0.003	28	11	5d ² 6s (³ F)	⁴ F _{5/2}	7305.09	5d ² 6p	53950.16(7/2)
44	21	2147.124	46559.28	-0.11	0.005	18	10	5d6s ²	² D _{5/2}	32063.81	5d6s6p	78623.20(7/2)
57	98	2147.199	46557.64	-0.04	0.002	17	8	5d ³	² G _{9/2}	12350.26	5d ² 6p	58907.94(9/2)
19	18	2150.466	46486.93	-0.02	0.001	29	15	5d ² 6s (³ F)	² F _{7/2}	17906.64	5d ² 6p	64393.59(7/2)
36	41	2158.101	46322.47	0.45	-0.021	14	14	5d ² 6s (³ P)	⁴ P _{1/2}	17030.94	5d ² 6p	63352.96(3/2)
54		2158.146	46321.52	-0.50	0.023						Hfs	
139	134	2158.438	46315.25	-0.02	0.001	14	13	5d ² 6s (³ F)	⁴ F _{9/2}	13766.13	5d ² 6p	60081.40(7/2)
6	3	2158.677	46310.12	-0.04	0.002	22	11	5d ³	² G _{7/2}	11296.10	5d ² 6p	57606.26(5/2)
6	2	2158.814	46307.19	-0.01	0.000	24	18	5d ³	² F _{5/2}	26854.64	5d ² 6p	73161.84(5/2)
21	14	2162.046	46237.97	0.00	0.000	19	12	5d6s ²	² D _{3/2}	28408.19	5d ² 6p	74646.16(3/2)
16	1	2162.431	46229.73	0.00	0.000	6	9	5d ³	¹ D _{3/2}	40470.77	5d6s6p	86700.50(3/2)
20	45	2162.647	46225.11	0.00	0.000	25	8	5d ² 6s (³ P)	⁴ P _{5/2}	20102.95	5d6s6p	66328.06(3/2)
11	1	2164.247	46190.95	0.34	-0.016	19	18	5d ² 6s (¹ G)	² G _{7/2}	26971.24	5d ² 6p	73161.84(5/2)
33	75	2164.667	46181.97	-0.04	0.002	18	9	5d6s ²	² D _{5/2}	32063.81	5d6s6p	78245.82(3/2)
7				0.22	-0.010	39	9	5d ³	³ D _{5/2}	12134.38	5d ² 6p	58316.13(3/2)
31	85	2166.313	46146.89	-0.03	0.002	29	17	5d ² 6s (³ F)	² F _{7/2}	17906.64	5d ² 6p	64053.56(5/2)
38	85	2169.157	46086.39	-0.03	0.002	23	15	5d ² 6s (³ P)	⁴ P _{3/2}	18777.41	5d ² 6p	64863.83(3/2)
48	98	2172.173	46022.42	-0.02	0.001	33	11	5d ² 6s (³ F)	² F _{5/2}	15719.85	5d ² 6p	61742.29(7/2)
24	9	2172.971	46005.52	-0.06	0.003	18	14	5d ³	² F _{7/2}	29375.47	5d ² 6p	75381.05(7/2)
17	20	2178.968	45878.92	-0.14	0.006	25	15	5d ² 6s (³ P)	⁴ P _{5/2}	20102.95	5d ² 6p	65982.01(7/2)
12	1	2179.100	45876.13	0.00	0.000	24	13	5d ² 6s (¹ D)	² D _{5/2}	25781.52	5d ² 6p	71657.65(3/2)
9	2	2181.384	45828.12	-0.05	0.003	32	12	5d ³	⁴ P _{5/2}	14365.56	5d ² 6p	60193.73(3/2)
15	47	2183.426	45785.26	-0.05	0.002	5	10	5d ³	² H _{11/2}	17553.75	5d ² 6p	63339.06(9/2)
67	41	2185.513	45741.53	0.02	-0.001	18	15	5d6s ²	² D _{5/2}	32063.81	5d ² 6p	77805.32(7/2)
5	1	2186.745	45715.76	-0.08	0.004	32	13	5d ³	⁴ P _{5/2}	14365.56	5d ² 6p	60081.40(7/2)
6	1	2195.276	45538.14	-0.07	0.003	15	10	5d ³	² H _{9/2}	17800.85	5d ² 6p	63339.06(9/2)
43	80	2200.384	45432.43	0.01	0.000	29	10	5d ² 6s (³ F)	² F _{7/2}	17906.64	5d ² 6p	63339.06(9/2)
25	4	2200.888	45422.03	0.01	-0.001	19	11	5d ² 6s (¹ G)	² G _{7/2}	26971.24	5d ² 6p	72393.26(9/2)
20	23	2202.286	45393.19	0.46	-0.022	14	9	5d ² 6s (³ P)	⁴ P _{1/2}	17030.94	5d ² 6p	62423.67(1/2)
36		2202.332	45392.25	-0.48	0.023						Hfs	
16	60	2207.980	45276.15	0.00	0.000	23	17	5d ² 6s (³ P)	⁴ P _{3/2}	18777.41	5d ² 6p	64053.56(5/2)
170	162	2214.541	45142.02	0.21	-0.010</							

Table I. Continued.

g_A (10^7 s^{-1})	Int	λ (Å)	$v(\text{cm}^{-1})$	$\Delta(v)^a$ (cm^{-1})	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark
14	1	2229.897	44831.18	0.00	0.000	19	15	$5d^26s (^1G)$	$^2G_{7/2}$ 26971.24	$5d^26p$ 71802.42(7/2)
90	98	2235.937	44710.09	0.13	-0.006	22	14	$5d^26s (^1D)$	$^2D_{3/2}$ 23796.27	$5d^26p$ 68506.23(5/2)
59	105	2242.681	44575.65	0.10	-0.005	23	14	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	$5d^26p$ 63352.96(3/2)
4	5	2247.822	44473.73	-0.15	0.008	33	12	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	$5d^26p$ 60193.73(3/2)
18	2	2247.860	44472.97	0.17	-0.009	13	15	$5d^26s (^1G)$	$^2G_{9/2}$ 27329.62	$5d^26p$ 71802.42(7/2)
4	1	2253.502	44361.63	0.08	-0.004	33	13	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	$5d^26p$ 60081.40(7/2)
7	47	2255.568	44321.00	-0.07	0.004	13	9	$5d^3$	$^2P_{1/2}$ 7882.85	$5d^26p$ 52203.92(3/2)
15	2	2257.112	44290.69	0.05	-0.003	25	15	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	$5d^26p$ 64393.59(7/2)
29	6	2262.153	44192.00	-0.03	0.002	6	10	$5d^3$	$^1D_{3/2}$ 40470.77	$5d^26p$ 84662.80(1/2)
19	60	2262.320	44188.74	0.03	-0.002	22	12	$5d^26s (^1D)$	$^2D_{3/2}$ 23796.27	$5d^26p$ 67984.98(3/2)
17	63	2267.228	44093.09	0.04	-0.002	22	13	$5d^3$	$^2G_{7/2}$ 11296.10	$5d^26p$ 55389.15(5/2)
23	45	2274.575	43950.67	0.06	-0.003	25	17	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	$5d^26p$ 64053.56(5/2)
56	98	2280.544	43835.66	0.01	-0.001	29	11	$5d^26s (^3F)$	$^2F_{7/2}$ 17906.64	$5d^26p$ 61742.29(7/2)
23	4	2283.108	43786.43	0.06	-0.003	18	18	$5d^3$	$^2F_{7/2}$ 29375.47	$5d^26p$ 73161.84(5/2)
19	30	2289.417	43665.78	-0.04	0.002	23	14	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	$5d^26p$ 62443.23(5/2)
26	6	2289.916	43656.27	-0.05	0.003	24	16	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 69437.84(7/2)
25	41	2290.444	43646.20	-0.06	0.004	23	9	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	$5d^26p$ 62423.67(1/2)
23	29	2292.050	43615.62	-0.01	0.000	24	12	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 69397.15(5/2)
120	147	2296.830	43524.85	-0.14	0.007	27	11	$5d^26s (^3F)$	$^4F_{7/2}$ 10425.17	$5d^26p$ 53950.16(7/2)
51	45	2307.837	43317.29	0.05	-0.003	18	14	$5d6s^2$	$^2D_{5/2}$ 32063.81	$5d^26p$ 75381.05(7/2)
71	98	2311.175	43254.74	-0.03	0.002	39	13	$5d^3$	$^2D_{5/2}$ 12134.38	$5d^26p$ 55389.15(5/2)
2	1	2311.448	43249.63	0.17	-0.009	19	13	$5d6s^2$	$^2D_{3/2}$ 28408.19	$5d^26p$ 71657.65(3/2)
6	1	2316.052	43163.66	0.87	-0.047	14	12	$5d^26s (^3P)$	$^4P_{1/2}$ 17030.94	$5d^26p$ 60193.73(3/2)
	1	2316.120	43162.40	-0.39	0.021					Hfs
14	1	2320.352	43083.67	0.01	0.000	14	13	$5d^26s (^3P)$	$^2P_{3/2}$ 36499.67	$5d^26p$ 79583.33(5/2)
309	123	2323.897	43017.96	0.17	-0.009	18	11	$5d^3$	$^2F_{7/2}$ 29375.47	$5d^26p$ 72393.26(9/2)
6	1	2327.594	42949.63	0.04	-0.002	24	15	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 68731.11(3/2)
2	1	2337.792	42762.29	0.01	-0.001	23	13	$5d^3$	$^2D_{3/2}$ 12626.87	$5d^26p$ 55389.15(5/2)
41	54	2338.642	42746.75	0.90	-0.049	14	4	$5d^26s (^3P)$	$^4P_{1/2}$ 17030.94	$5d^26p$ 59776.79(1/2)
	63	2338.710	42745.51	-0.34	0.019					Hfs
149	202	2343.649	42655.46	0.00	0.000	27	7	$5d^26s (^3F)$	$^4F_{3/2}$ 5542.39	$5d^26p$ 48197.85(5/2)
22	57	2346.901	42596.34	0.06	-0.004	33	9	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	$5d^26p$ 58316.13(3/2)
78	67	2347.627	42583.16	-0.04	0.002	24	16	$5d^3$	$^2F_{5/2}$ 26854.64	$5d^26p$ 69437.84(7/2)
75	80	2354.072	42466.59	-0.01	0.001	19	16	$5d^26s (^1G)$	$^2G_{7/2}$ 26971.24	$5d^26p$ 69437.84(7/2)
20	7	2361.095	42340.28	0.00	0.000	25	14	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	$5d^26p$ 62443.23(5/2)
8	2	2364.431	42280.56	0.01	0.000	15	13	$5d^3$	$^2H_{9/2}$ 17800.85	$5d^26p$ 60081.40(7/2)
17	1	2368.757	42203.34	-0.12	0.007	24	12	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 67984.98(3/2)
62	98	2370.362	42174.78	0.02	-0.001	29	13	$5d^26s (^3F)$	$^2F_{7/2}$ 17906.64	$5d^26p$ 60081.40(7/2)
59	29	2374.104	42108.30	0.08	-0.005	13	16	$5d^26s (^1G)$	$^2G_{9/2}$ 27329.62	$5d^26p$ 69437.84(7/2)
5	1	2384.799	41919.47	0.02	-0.001	18	13	$5d6s^2$	$^2D_{5/2}$ 32063.81	$5d6s6p$ 73983.26(7/2)
9	1	2387.241	41876.59	0.12	-0.007	24	15	$5d^3$	$^2F_{5/2}$ 26854.64	$5d^26p$ 68731.11(3/2)
13	57	2390.713	41815.79	0.00	0.000	39	11	$5d^3$	$^2D_{5/2}$ 12134.38	$5d^26p$ 53950.16(7/2)
59	63	2394.698	41746.21	0.06	-0.004	14	9	$5d^26s (^3P)$	$^2P_{3/2}$ 36499.67	$5d^26p$ 78245.82(3/2)
73	71	2397.760	41692.89	0.09	-0.005	10	12	$5d^26s (^3P)$	$^2P_{1/2}$ 32953.36	$5d^26p$ 74646.16(3/2)
6	1	2403.113	41600.04	0.14	-0.008	17	11	$5d^3$	$^2G_{9/2}$ 12350.26	$5d^26p$ 53950.16(7/2)
5	1	2413.773	41416.33	0.01	0.000	23	12	$5d^26s (^3P)$	$^4P_{3/2}$ 18777.41	$5d^26p$ 60193.73(3/2)
8	1	2417.404	41354.12	-0.07	0.004	5	8	$5d^3$	$^2H_{11/2}$ 17553.75	$5d^26p$ 58907.94(9/2)
106	85	2428.498	41165.22	0.05	-0.003	19	10	$5d^26s (^1G)$	$^2G_{7/2}$ 26971.24	$5d^26p$ 68136.41(9/2)
8	16	2436.892	41023.43	-0.16	0.009	32	13	$5d^3$	$^4P_{5/2}$ 14365.56	$5d^26p$ 55389.15(5/2)
11	14	2437.638	41010.88	0.00	0.000	28	7	$5d^3$	$^2P_{3/2}$ 7186.97	$5d^26p$ 48197.85(5/2)
62	98	2438.208	41001.29	-0.01	0.001	29	8	$5d^26s (^3F)$	$^2F_{7/2}$ 17906.64	$5d^26p$ 58907.94(9/2)
65	147	2444.688	40892.62	-0.14	0.009	28	7	$5d^26s (^3F)$	$^4F_{5/2}$ 7305.09	$5d^26p$ 48197.85(5/2)
92	8	2449.838	40806.67	-0.12	0.007	13	10	$5d^26s (^1G)$	$^2G_{9/2}$ 27329.62	$5d^26p$ 68136.41(9/2)
18	3	2466.656	40528.46	-0.50	0.031	24	13	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 66310.48(5/2)
74	6	2472.329	40435.47	-0.52	0.032	14	17	$5d^26s (^3P)$	$^2P_{3/2}$ 36499.67	$5d^26p$ 76935.66(5/2)
19	10	2479.215	40323.17	0.25	-0.015	19	15	$5d6s^2$	$^2D_{3/2}$ 28408.19	$5d^26p$ 68731.11(3/2)
2	5	2486.813	40199.98	-0.51	0.031	24	15	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 65982.01(7/2)
29	2	2493.140	40097.97	-0.07	0.005	19	14	$5d6s^2$	$^2D_{3/2}$ 28408.19	$5d^26p$ 68506.23(5/2)
14	2	2493.560	40091.22	0.44	-0.027	25	12	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	$5d^26p$ 60193.73(3/2)
7	10	2520.082	39669.31	0.01	-0.001	33	13	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	$5d^26p$ 55389.15(5/2)
12	5	2523.904	39609.24	-0.15	0.010	10	6	$5d^26s (^3P)$	$^2P_{1/2}$ 32953.36	$5d^26p$ 72562.75(1/2)
9	6	2525.498	39584.25	-0.35	0.022	32	11	$5d^3$	$^4P_{5/2}$ 14365.56	$5d^26p$ 53950.16(7/2)
20	6	2562.628	39010.75	-0.02	0.001	19	15	$5d^26s (^1G)$	$^2G_{7/2}$ 26971.24	$5d^26p$ 65982.01(7/2)
20	10	2586.410	38652.07	-0.32	0.021	13	15	$5d^26s (^1G)$	$^2G_{9/2}$ 27329.62	$5d^26p$ 65982.01(7/2)
6	4	2588.078	38627.16	-0.24	0.016	22	9	$5d^26s (^1D)$	$^2D_{3/2}$ 23796.27	$5d^26p$ 62423.67(1/2)
13	3	2589.117	38611.66	-0.41	0.028	24	15	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 64393.59(7/2)
20	25	2614.942	38230.35	0.04	-0.003	33	11	$5d^26s (^3F)$	$^2F_{5/2}$ 15719.85	$5d^26p$ 53950.16(7/2)
2	2	2616.115	38213.21	0.03	-0.002	25	9	$5d^26s (^3P)$	$^4P_{5/2}$ 20102.95	$5d^26p$ 58316.13(3/2)
11	3	2630.182	38008.85	-0.34	0.024	24	15	$5d^3$	$^2F_{5/2}$ 26854.64	$5d^26p$ 64863.83(3/2)
3	3	2642.056	37838.04	-0.32	0.022	32	9	$5d^3$	$^4P_{5/2}$ 14365.56	$5d^26p$ 52203.92(3/2)
4	3	2660.810	37571.36	-0.08	0.006	24	14	$5d^26s (^1D)$	$^2D_{5/2}$ 25781.52	$5d^26p$ 63352.96(3/2)
6	10	2663.074	37539.42	0.47	-0.034	24	15	$5d^3$	$^2F_{5/2}$ 26854.64	$5d^26p$ 64393.59(7/2)
5	50	2665.6								

Table I. *Continued.*

g_A (10^7 s^{-1})	Int	λ (Å)	v(cm ⁻¹)	$\Delta(v)^a$ (cm ⁻¹)	$\Delta(\lambda)^a$ (Å)	N_{even}^b	N_{odd}^b	Even level	Odd level	Remark
1	4	2726.852	36661.47	-0.24	0.018	24	14	$5d^26s (^1D)$	$^2D_{5/2}$	25781.52
5	2	2730.976	36606.11	-0.43	0.032	18	15	$5d^3$	$^2F_{7/2}$	29375.47
1	2	2737.199	36522.89	0.07	-0.005	26	9	$5d^3$	$^4P_{3/2}$	15681.10
9	25	2740.110	36484.09	0.02	-0.002	33	9	$5d^26s (^3F)$	$^2F_{5/2}$	15719.85
2	15	2742.234	36455.83	0.19	-0.014	19	15	$5d6s^2$	$^2D_{3/2}$	28408.19
2	2	2772.056	36063.66	0.19	-0.015	39	7	$5d^3$	$^2D_{5/2}$	12134.38
4	5	2773.595	36043.65	0.13	-0.010	29	11	$5d^26s (^3F)$	$^2F_{7/2}$	17906.64
11	5	2776.231	36009.42	-0.02	0.001	13	10	$5d^26s (^1G)$	$^2G_{9/2}$	27329.62
1	3	2804.580	35645.46	0.09	-0.007	19	17	$5d6s^2$	$^2D_{3/2}$	28408.19
1	6	2854.786	35018.60	0.48	-0.039	18	15	$5d^3$	$^2F_{7/2}$	29375.47
4	8	2882.826	34678.01	-0.08	0.006	18	17	$5d^3$	$^2F_{7/2}$	29375.47
4	7	2896.041	34519.78	-0.08	0.006	22	9	$5d^26s (^1D)$	$^2D_{3/2}$	23796.27
5	5	2943.482	33963.44	-0.15	0.013	18	10	$5d^3$	$^2F_{7/2}$	29375.47
2	8	2954.921	33831.97	-0.32	0.028	32	7	$5d^3$	$^4P_{5/2}$	14365.56
5	100	2956.835	33810.07	0.08	-0.007	22	11	$5d^26s (^1D)$	$^2D_{3/2}$	23796.27
4	8	3019.336	33110.22	0.06	-0.005	19	13	$5d^26s (^1G)$	$^2G_{7/2}$	26971.24
4	5	3023.202	33067.88	0.12	-0.011	18	14	$5d^3$	$^2F_{7/2}$	29375.47
6	25	3078.097	32478.17	0.17	-0.016	33	7	$5d^26s (^3F)$	$^2F_{5/2}$	15719.85
7	10	3088.692	32366.77	-0.05	0.005	18	11	$5d^3$	$^2F_{7/2}$	29375.47
1	3	3132.861	31910.46	-0.01	0.001	10	15	$5d^26s (^3P)$	$^2P_{1/2}$	32953.36
3	15	3164.345	31592.97	0.09	-0.009	22	13	$5d^26s (^1D)$	$^2D_{3/2}$	23796.27
5	10	3177.564	31461.55	0.06	-0.006	24	9	$5d^3$	$^2F_{5/2}$	26854.64
4	12	3255.760	30705.94	0.01	-0.001	18	13	$5d^3$	$^2F_{7/2}$	29375.47
4	10	3288.566	30399.63	0.03	-0.004	10	14	$5d^26s (^3P)$	$^2P_{1/2}$	32953.36
4	12	3290.764	30379.33	-0.09	0.010	18	14	$5d6s^2$	$^2D_{5/2}$	32063.81
1	6	3524.550	28364.31	0.15	-0.019	14	15	$5d^26s (^3P)$	$^2P_{3/2}$	36499.67
2	10	3569.817	28004.64	0.10	-0.013	10	5	$5d^26s (^3P)$	$^2P_{1/2}$	32953.36
2	8	3689.597	27095.52	0.00	0.000	24	11	$5d^3$	$^2F_{5/2}$	26854.64
2	2	3843.023	26013.80	0.12	-0.018	18	13	$5d^3$	$^2F_{7/2}$	29375.47
2	10	3856.328	25924.05	0.05	-0.008	14	9	$5d^26s (^3P)$	$^2P_{3/2}$	36499.67
2	10	3943.777	25349.23	-0.05	0.008	24	9	$5d^3$	$^2F_{5/2}$	26854.64

^a $\Delta(x)$ = Difference between the observed and calculated (derived from the level energies) values of x .^b $N_{\text{odd}}, N_{\text{even}}$ = The number of observed transitions from (to) the level involved, respectively.

c Lines are from Ref. [9]

d Lines are from Ref. [3]

M = The Ta III line is masked by some other line.

Str = The intensity of the line is too strong compared to expected (2–3 times).

Bl = The line is blended by a close line.

Hfs = Hyperfine splitting of the $5d^26s (^3P) ^4P_{1/2}$ energy level at 17030.94 cm^{-1} .F= F -values correspond to the two hfs sublevels (43279.83 cm^{-1} and 43281.99 cm^{-1}) of the $5d^26s (^1S) ^2S_{1/2}$ energy level.

structures (hfs) which have been interpreted theoretically [24]. The magnetic hfs constants in the low even group ($5d + 6s$)⁵ are expressed in terms of adjustable mono-electronic parameters a_{5d}^{kk} and a_{6s}^{10} which dominates the former ones by a factor of twenty. As concerns ions of the 5d-elements, Fourier Transform spectrometry (FTS) resumed high resolution studies, which were initiated long ago by Fabry–Perot interferometry, but results on Ta III did not appear so far. Semi-empirical considerations help to evaluate the sizes of the structures in the present work. The mono-electronic parameters scale as $\langle r^{-3} \rangle$ and are expected to increase with ionic charge. This trend is confirmed in the nearby element $_{71}\text{Lu}$. FTS analysis of Lu I [25] and subsequent interpretation of ($5d + 6s$)³ and ($5d + 6s$)²6p led to $a_{6s}^{10} = 0.275 \pm 0.002 \text{ cm}^{-1}$ [26]. The observation of the Lu III 6s²S–6p²P doublet on the 10.7 m spectrograph at the National Bureau of Standards (NBS) (similar to the one in Meudon, with a 1200 lines/mm ruled grating) led Kaufman and Sugar to $0.436 \pm 0.002 \text{ cm}^{-1}$ for the same parameter [27]. In Lu II, Gollnow derived intermediate values 0.362 cm^{-1} from 6s6p and 0.320 cm^{-1} from 5d6s [28]. In Ta I, a value $a_{6s}^{10} = 0.306 \pm 0.005 \text{ cm}^{-1}$ is derived in [24] and for Ta II Murakawa obtained $0.405 \pm 0.005 \text{ cm}^{-1}$ from the A -con-

stant of the ground level $5d^36s ^5F_1$ [29], in agreement with *ab initio* studies [30], provided that the results are scaled from nuclear spin $I = 3/2$ to $I = 7/2$. Recent refinement of the energy level structure of Ta II and careful analysis of hfs patterns of Ta II by means of FTS resulted in a list of well defined hfs constants for 105 levels [31]. These

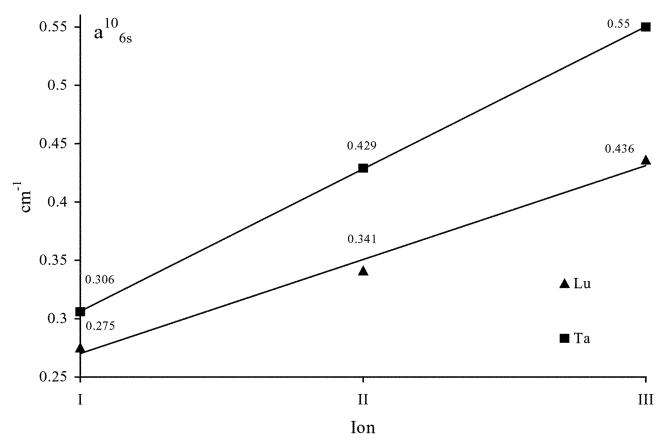
Fig. 1. Estimation of an a_{6s}^{10} value for Ta III. Data on Lu I – Lu III, Ta I and Ta II are used.

Table II. Experimental and calculated energy levels (cm^{-1}) in the $5d^3$, $5d^26s$ and $5d6s^2$ configurations of Ta III.

E_{obs}	E_{calc}	Δ^{a}	N^{b}	rms	g^{c}	Composition ^d										
<i>J = 0.5</i>																
43281.18	43381.08	-99.90	4	0.13	1.938	92%	2 (${}^1_0\text{S}$) ${}^2\text{S}$	+	5%	2 (${}^3_2\text{P}$) ${}^2\text{P}$	+	2%	2 (${}^3_2\text{P}$) ${}^4\text{P}$			
32953.36	33013.01	-59.65	10	0.10	0.757	71%	2 (${}^3_2\text{P}$) ${}^2\text{P}$	+	23%	1 (${}^3_1\text{P}$) ${}^2\text{P}$	+	5%	2 (${}^1_0\text{S}$) ${}^2\text{S}$			
17030.94	17122.01	-91.07	14	0.30	2.639	97%	2 (${}^3_2\text{P}$) ${}^4\text{P}$	+	3%	2 (${}^1_0\text{S}$) ${}^2\text{S}$	+	1%	1 (${}^3_1\text{P}$) ${}^2\text{P}$			
12805.56	12786.25	19.31	10	0.06	2.215	77%	1 (${}^4_3\text{P}$)	+	15%	1 (${}^3_1\text{P}$) ${}^2\text{P}$	+	8%	2 (${}^3_2\text{P}$) ${}^2\text{P}$			
7882.85	7849.07	33.78	13	0.06	1.126	60%	1 (${}^4_3\text{P}$)	+	23%	1 (${}^4_3\text{P}$)	+	17%	2 (${}^3_2\text{P}$) ${}^2\text{P}$			
<i>J = 1.5</i>																
40470.77	40426.30	44.47	6	0.05	0.808	51%	1 (${}^2_1\text{D}$)	+	28%	3 (${}^2_1\text{D}$)	+	17%	1 (${}^2_3\text{D}$)			
36499.67	36477.56	22.11	14	0.14	1.295	69%	2 (${}^3_2\text{P}$) ${}^2\text{P}$	+	22%	1 (${}^2_3\text{P}$)	+	4%	2 (${}^1_2\text{D}$) ${}^2\text{D}$			
28408.19	28428.15	-19.96	19	0.08	0.810	53%	3 (${}^2_1\text{D}$)	+	17%	1 (${}^2_1\text{D}$)	+	16%	2 (${}^1_2\text{D}$) ${}^2\text{D}$			
23796.27	23735.69	60.58	22	0.07	0.839	46%	2 (${}^1_2\text{D}$) ${}^2\text{D}$	+	30%	1 (${}^2_3\text{D}$)	+	8%	3 (${}^2_1\text{D}$)			
18777.41	18811.59	-34.18	23	0.05	1.687	93%	2 (${}^3_2\text{P}$) ${}^4\text{P}$	+	2%	1 (${}^2_3\text{D}$)	+	2%	1 (${}^2_3\text{P}$)			
15681.10	15778.66	-97.56	26	0.06	1.385	35%	1 (${}^4_3\text{P}$)	+	30%	1 (${}^2_3\text{P}$)	+	13%	2 (${}^3_2\text{P}$) ${}^2\text{P}$			
12626.87	12689.94	-63.07	23	0.06	1.171	42%	1 (${}^4_3\text{P}$)	+	19%	1 (${}^2_3\text{D}$)	+	15%	2 (${}^1_2\text{D}$) ${}^2\text{D}$			
7186.97	7164.23	22.74	28	0.06	1.073	34%	1 (${}^4_3\text{P}$)	+	27%	2 (${}^3_2\text{F}$) ${}^4\text{F}$	+	19%	1 (${}^4_3\text{P}$)			
5542.39	5539.41	2.98	27	0.08	0.597	66%	2 (${}^3_2\text{F}$) ${}^4\text{F}$	+	9%	2 (${}^1_2\text{D}$) ${}^2\text{D}$	+	8%	1 (${}^2_3\text{P}$)			
0.00	21.68	-21.68	16	0.07	0.469	85%	1 (${}^4_3\text{F}$)	+	7%	1 (${}^2_3\text{D}$)	+	4%	1 (${}^2_1\text{D}$)			
<i>J = 2.5</i>																
42619.53	42655.48	-35.95	4	0.08	1.197	49%	3 (${}^2_1\text{D}$)	+	42%	1 (${}^2_3\text{D}$)	+	4%	1 (${}^2_3\text{D}$)			
32063.81	32002.27	61.54	18	0.07	1.131	31%	3 (${}^2_1\text{D}$)	+	29%	1 (${}^1_1\text{D}$)	+	17%	1 (${}^2_3\text{F}$)			
26854.64	26890.01	-35.37	24	0.06	0.973	48%	1 (${}^2_3\text{F}$)	+	19%	2 (${}^3_2\text{F}$) ${}^2\text{F}$	+	12%	1 (${}^2_1\text{D}$)			
25781.52	25684.16	97.36	24	0.06	1.219	40%	2 (${}^1_2\text{D}$) ${}^2\text{D}$	+	27%	1 (${}^2_3\text{D}$)	+	14%	2 (${}^3_2\text{P}$) ${}^4\text{P}$			
20102.95	20071.75	31.20	25	0.08	1.513	78%	2 (${}^3_2\text{P}$) ${}^4\text{P}$	+	16%	1 (${}^2_3\text{D}$)	+	3%	1 (${}^2_1\text{D}$)			
15719.85	15688.00	31.85	33	0.05	0.995	51%	2 (${}^3_2\text{F}$) ${}^2\text{F}$	+	16%	1 (${}^2_3\text{F}$)	+	14%	1 (${}^2_3\text{D}$)			
14365.56	14315.01	50.55	32	0.09	1.452	75%	1 (${}^4_3\text{P}$)	+	11%	2 (${}^3_2\text{F}$) ${}^2\text{F}$	+	5%	2 (${}^1_2\text{D}$) ${}^2\text{D}$			
12134.38	12222.26	-87.88	39	0.07	1.222	21%	2 (${}^1_2\text{D}$) ${}^2\text{D}$	+	19%	1 (${}^2_3\text{D}$)	+	18%	1 (${}^4_3\text{P}$)			
7305.09	7331.65	-26.56	28	0.07	1.037	81%	2 (${}^3_2\text{F}$) ${}^4\text{F}$	+	8%	2 (${}^1_2\text{D}$) ${}^2\text{D}$	+	7%	2 (${}^3_2\text{F}$) ${}^2\text{F}$			
2512.43	2524.45	-12.02	17	0.07	1.036	96%	1 (${}^4_3\text{F}$)	+	3%	1 (${}^2_3\text{D}$)	+	1%	1 (${}^2_1\text{D}$)			
<i>J = 3.5</i>																
29375.47	29496.16	-120.69	18	0.09	1.111	43%	2 (${}^3_2\text{F}$) ${}^2\text{F}$	+	43%	1 (${}^2_3\text{F}$)	+	13%	2 (${}^1_2\text{G}$) ${}^2\text{G}$			
26971.24	26901.47	69.77	19	0.05	0.930	76%	2 (${}^1_2\text{G}$) ${}^2\text{G}$	+	15%	1 (${}^2_3\text{F}$)	+	8%	1 (${}^2_3\text{G}$)			
17906.64	17851.33	55.31	29	0.06	1.135	52%	2 (${}^3_2\text{F}$) ${}^2\text{F}$	+	40%	1 (${}^2_3\text{F}$)	+	4%	2 (${}^1_2\text{G}$) ${}^2\text{G}$			
11296.10	11304.21	-8.11	22	0.06	0.953	76%	1 (${}^2_3\text{G}$)	+	12%	2 (${}^3_2\text{F}$) ${}^4\text{F}$	+	6%	1 (${}^4_3\text{F}$)			
10425.17	10418.78	6.39	27	0.07	1.197	84%	2 (${}^3_2\text{F}$) ${}^4\text{F}$	+	9%	1 (${}^2_3\text{G}$)	+	3%	2 (${}^3_2\text{F}$) ${}^2\text{F}$			
4854.18	4854.23	-0.05	18	0.07	1.215	93%	1 (${}^4_3\text{F}$)	+	6%	1 (${}^2_3\text{G}$)	+	1%	1 (${}^2_3\text{F}$)			
<i>J = 4.5</i>																
27329.62	27315.63	13.99	13	0.08	1.115	85%	2 (${}^1_2\text{G}$) ${}^2\text{G}$	+	11%	1 (${}^2_3\text{G}$)	+	2%	2 (${}^3_2\text{F}$) ${}^4\text{F}$			
17800.85	17826.57	-25.72	15	0.06	1.015	54%	1 (${}^2_3\text{H}$)	+	33%	1 (${}^2_3\text{G}$)	+	7%	2 (${}^1_2\text{G}$) ${}^2\text{G}$			
13766.13	13780.35	-14.22	14	0.06	1.293	88%	2 (${}^3_2\text{F}$) ${}^4\text{F}$	+	8%	1 (${}^2_3\text{H}$)	+	2%	1 (${}^2_3\text{G}$)			
12350.26	12310.26	40.00	17	0.07	1.100	35%	1 (${}^2_3\text{H}$)	+	34%	1 (${}^2_3\text{G}$)	+	19%	1 (${}^4_3\text{F}$)			
6776.24	6759.70	16.54	15	0.07	1.277	77%	1 (${}^4_3\text{F}$)	+	20%	1 (${}^2_3\text{G}$)	+	3%	1 (${}^2_3\text{H}$)			
<i>J = 5.5</i>																
17553.75	17557.70	-3.95	5	0.05	1.091	100%	1 (${}^2_3\text{H}$)									

^a $\Delta = (E_{\text{obs}} - E_{\text{calc}})$.

^b N = The number of spectral lines used to determine the energy level value.

^c g = The calculated Landé factor.

^d The number preceding the term name has the following meaning: 1 stands for $5d^3$, 2 stands for $5d^26s$, and 3 stands for $5d6s^2$.

constants determine a new value, $a_{6s}^{10} = 0.429 \pm 0.01 \text{ cm}^{-1}$, for Ta II. All these data were used to estimate a a_{6s}^{10} value in Ta III (see Fig. 1). For Lu II we used a value of 0.341 cm^{-1} which is the average of those two published [28]. The regular trends that can be seen in Fig. 1 lead to an expected value $a_{6s}^{10} = 0.55 \pm 0.01 \text{ cm}^{-1}$ in Ta III, and for the level $5d^26s^2S_{1/2}$ the hfs splitting is $4 \times a_{6s}^{10} = 2.20 \text{ cm}^{-1}$. This is consistent with the present observations. The search for the level $5d^26s^2S_{1/2}$ leads to the two values $43279.83 \pm 0.05 \text{ cm}^{-1}$ and $43281.99 \pm 0.08 \text{ cm}^{-1}$ corresponding to hfs transitions towards $F = 3$ and $F = 4$ of ${}^2S_{1/2}$ sublevels respectively. The derived value of the ${}^2S_{1/2}$

level and the value of the splitting are $43281.18 \pm 0.13 \text{ cm}^{-1}$ and $2.18 \pm 0.11 \text{ cm}^{-1}$. Due to different C.I. effects and coupling conditions, comparisons of Ta III with Lu I are not straightforward. It is noticed that two other levels ($5d^26s^4P_{1/2}$ and $5d6s6p^4P_{1/2}$) have prominent A constants in Lu I. In Ta III the former of both levels (17030.94 cm^{-1}) has partially resolved hfs transitions, doublet-like with average separation of $1.14 \pm 0.15 \text{ cm}^{-1}$. Other transitions with larger J -values and smaller A constants are expected to have more complex hfs patterns which contribute to the asymmetry of several lines and merge into wavenumber uncertainties.

Table III. Experimental and calculated energy levels (cm^{-1}) in the $5d^26p$, $5d6s6p$ and $6s^26p$ configurations of Ta III.

E_{obs}	E_{calc}	Δ^{a}	N^{b}	rms	g^{c}	Composition ^d							
<i>J = 0.5</i>													
—	106306.69	—	—	—	0.665	55%	3 (${}^1\text{S}$) ${}^2\text{P}$	+	31%	2 (${}^3\text{D}$) ${}^2\text{P}$	+	5%	1 (${}^3\text{P}$) ${}^2\text{P}$
101164.31	100893.35	270.96	6	0.10	0.667	52%	2 (${}^1\text{D}$) ${}^2\text{P}$	+	16%	3 (${}^1\text{S}$) ${}^2\text{P}$	+	10%	1 (${}^1\text{S}$) ${}^2\text{P}$
91302.20	91492.10	-189.90	4	0.16	0.703	36%	1 (${}^1\text{S}$) ${}^2\text{P}$	+	29%	2 (${}^3\text{D}$) ${}^2\text{P}$	+	27%	2 (${}^1\text{D}$) ${}^2\text{P}$
84662.80	84813.71	-150.91	10	0.08	0.702	42%	1 (${}^3\text{P}$) ${}^2\text{P}$	+	18%	3 (${}^1\text{S}$) ${}^2\text{P}$	+	17%	1 (${}^1\text{S}$) ${}^2\text{P}$
79281.40	79267.91	13.49	2	0.20	2.509	85%	2 (${}^3\text{D}$) ${}^4\text{P}$	+	7%	1 (${}^3\text{P}$) ${}^4\text{P}$	+	2%	2 (${}^3\text{D}$) ${}^4\text{D}$
75150.55	75098.39	52.16	4	0.12	0.658	24%	1 (${}^1\text{S}$) ${}^2\text{P}$	+	23%	1 (${}^3\text{P}$) ${}^2\text{P}$	+	11%	1 (${}^1\text{D}$) ${}^2\text{P}$
72562.75	72599.79	-37.04	6	0.09	1.846	45%	1 (${}^3\text{P}$) ${}^4\text{P}$	+	17%	1 (${}^3\text{P}$) ${}^2\text{S}$	+	11%	1 (${}^1\text{D}$) ${}^2\text{P}$
69517.83	69554.96	-37.13	4	0.07	0.613	38%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	19%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	10%	1 (${}^3\text{P}$) ${}^4\text{P}$
68758.14	68632.37	125.77	8	0.07	0.668	40%	1 (${}^1\text{D}$) ${}^2\text{P}$	+	33%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	11%	1 (${}^3\text{P}$) ${}^4\text{P}$
62423.67	62383.42	40.25	9	0.05	0.624	51%	1 (${}^3\text{P}$) ${}^4\text{D}$	+	19%	1 (${}^3\text{P}$) ${}^2\text{S}$	+	7%	1 (${}^3\text{P}$) ${}^4\text{P}$
60957.90	61089.48	-131.58	5	0.07	1.076	38%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	30%	1 (${}^3\text{P}$) ${}^2\text{S}$	+	15%	1 (${}^3\text{P}$) ${}^4\text{P}$
59776.79	59496.78	280.01	4	0.05	0.599	31%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	29%	1 (${}^3\text{P}$) ${}^4\text{D}$	+	19%	1 (${}^3\text{P}$) ${}^2\text{S}$
<i>J = 1.5</i>													
—	115140.86	—	—	—	1.334	74%	3 (${}^1\text{S}$) ${}^2\text{P}$	+	19%	2 (${}^3\text{D}$) ${}^2\text{P}$	+	5%	1 (${}^1\text{S}$) ${}^2\text{P}$
106246.27	106191.14	55.13	9	0.14	1.326	32%	2 (${}^3\text{D}$) ${}^2\text{P}$	+	23%	2 (${}^1\text{D}$) ${}^2\text{P}$	+	20%	1 (${}^1\text{S}$) ${}^2\text{P}$
95641.00	95841.87	-200.87	13	0.10	0.955	35%	2 (${}^1\text{D}$) ${}^2\text{D}$	+	19%	2 (${}^3\text{D}$) ${}^2\text{D}$	+	13%	2 (${}^1\text{D}$) ${}^2\text{P}$
91729.46	91743.11	-13.65	14	0.10	1.181	41%	1 (${}^1\text{S}$) ${}^2\text{P}$	+	20%	2 (${}^3\text{D}$) ${}^2\text{D}$	+	14%	2 (${}^1\text{D}$) ${}^2\text{P}$
86700.50	86479.98	220.52	9	0.07	1.328	23%	2 (${}^3\text{D}$) ${}^2\text{P}$	+	16%	2 (${}^3\text{D}$) ${}^4\text{P}$	+	15%	1 (${}^1\text{S}$) ${}^2\text{P}$
81593.82	81734.80	-140.98	11	0.10	0.890	35%	1 (${}^1\text{D}$) ${}^2\text{D}$	+	21%	2 (${}^3\text{D}$) ${}^2\text{D}$	+	16%	2 (${}^1\text{D}$) ${}^2\text{P}$
78799.45	78838.10	-38.65	7	0.08	1.552	53%	2 (${}^3\text{D}$) ${}^4\text{P}$	+	12%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	12%	2 (${}^3\text{D}$) ${}^2\text{P}$
78245.82	78320.33	-74.51	9	0.08	1.346	54%	1 (${}^3\text{P}$) ${}^2\text{P}$	+	15%	2 (${}^3\text{D}$) ${}^4\text{P}$	+	8%	2 (${}^1\text{D}$) ${}^2\text{D}$
74646.16	74660.57	-14.41	12	0.07	0.950	60%	1 (${}^3\text{P}$) ${}^2\text{D}$	+	12%	2 (${}^1\text{D}$) ${}^2\text{D}$	+	7%	1 (${}^3\text{P}$) ${}^2\text{P}$
72185.94	72033.26	152.68	6	0.05	1.520	45%	1 (${}^3\text{P}$) ${}^4\text{P}$	+	32%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	10%	1 (${}^3\text{P}$) ${}^4\text{S}$
71657.65	71589.72	67.93	13	0.07	1.285	29%	1 (${}^1\text{D}$) ${}^2\text{P}$	+	17%	1 (${}^3\text{P}$) ${}^4\text{S}$	+	14%	2 (${}^3\text{D}$) ${}^4\text{D}$
68731.11	68727.73	3.38	15	0.08	1.339	23%	1 (${}^3\text{P}$) ${}^4\text{P}$	+	17%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	15%	1 (${}^1\text{D}$) ${}^2\text{P}$
67984.98	68105.81	-120.83	12	0.05	1.309	44%	1 (${}^3\text{P}$) ${}^4\text{S}$	+	22%	2 (${}^3\text{D}$) ${}^4\text{F}$	+	15%	1 (${}^1\text{D}$) ${}^2\text{D}$
66328.06	66125.52	202.54	8	0.05	0.988	28%	2 (${}^3\text{D}$) ${}^4\text{F}$	+	25%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	20%	1 (${}^3\text{P}$) ${}^4\text{D}$
64863.83	64977.46	-113.63	15	0.05	1.002	27%	2 (${}^3\text{D}$) ${}^4\text{F}$	+	26%	1 (${}^3\text{P}$) ${}^4\text{D}$	+	9%	1 (${}^3\text{P}$) ${}^4\text{S}$
63352.96	63310.82	42.14	14	0.06	1.045	28%	1 (${}^3\text{P}$) ${}^4\text{D}$	+	24%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	10%	1 (${}^3\text{F}$) ${}^2\text{D}$
60193.73	60243.61	-49.88	12	0.07	1.069	28%	1 (${}^1\text{D}$) ${}^2\text{P}$	+	23%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	19%	1 (${}^3\text{F}$) ${}^4\text{D}$
58316.13	58386.77	-70.64	9	0.06	0.814	27%	1 (${}^1\text{D}$) ${}^2\text{D}$	+	23%	1 (${}^3\text{F}$) ${}^2\text{D}$	+	12%	1 (${}^3\text{F}$) ${}^4\text{F}$
52203.92	52273.03	-69.11	9	0.08	0.640	51%	1 (${}^3\text{F}$) ${}^4\text{F}$	+	30%	1 (${}^3\text{F}$) ${}^2\text{D}$	+	7%	1 (${}^3\text{F}$) ${}^4\text{D}$
<i>J = 2.5</i>													
100370.33	100356.80	13.53	10	0.20	1.154	36%	2 (${}^3\text{D}$) ${}^2\text{D}$	+	33%	2 (${}^1\text{D}$) ${}^2\text{D}$	+	11%	1 (${}^3\text{F}$) ${}^2\text{D}$
95997.96	96153.84	-155.88	12	0.11	0.904	54%	2 (${}^3\text{D}$) ${}^2\text{F}$	+	18%	1 (${}^1\text{G}$) ${}^2\text{F}$	+	10%	2 (${}^1\text{D}$) ${}^2\text{F}$
88212.38	88103.23	109.15	14	0.15	1.062	37%	2 (${}^1\text{D}$) ${}^2\text{F}$	+	12%	2 (${}^3\text{D}$) ${}^2\text{D}$	+	12%	1 (${}^1\text{D}$) ${}^2\text{D}$
83196.94	83334.93	-137.99	13	0.15	1.185	34%	2 (${}^1\text{D}$) ${}^2\text{F}$	+	27%	2 (${}^3\text{D}$) ${}^4\text{P}$	+	10%	1 (${}^1\text{D}$) ${}^2\text{D}$
79583.33	79406.29	177.04	13	0.05	1.043	45%	1 (${}^1\text{G}$) ${}^2\text{F}$	+	13%	2 (${}^3\text{D}$) ${}^4\text{P}$	+	11%	2 (${}^3\text{D}$) ${}^2\text{F}$
78770.02	78884.15	-114.13	12	0.16	1.278	36%	2 (${}^3\text{D}$) ${}^4\text{P}$	+	20%	1 (${}^1\text{D}$) ${}^2\text{D}$	+	17%	1 (${}^1\text{G}$) ${}^2\text{F}$
76935.66	76921.80	13.86	17	0.06	1.273	40%	1 (${}^3\text{P}$) ${}^2\text{D}$	+	31%	1 (${}^3\text{P}$) ${}^4\text{P}$	+	11%	1 (${}^1\text{G}$) ${}^2\text{F}$
75180.08	75046.17	133.91	9	0.06	1.383	46%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	20%	1 (${}^3\text{P}$) ${}^4\text{P}$	+	15%	1 (${}^3\text{P}$) ${}^4\text{D}$
73161.84	73202.85	-41.01	18	0.08	1.369	28%	1 (${}^3\text{P}$) ${}^4\text{P}$	+	22%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	12%	1 (${}^3\text{P}$) ${}^2\text{D}$
70163.46	70002.37	161.09	10	0.09	1.171	46%	2 (${}^3\text{D}$) ${}^4\text{F}$	+	18%	1 (${}^3\text{F}$) ${}^2\text{D}$	+	12%	1 (${}^3\text{P}$) ${}^4\text{D}$
69397.15	69506.07	-108.92	12	0.05	1.264	45%	1 (${}^3\text{P}$) ${}^4\text{D}$	+	16%	2 (${}^3\text{D}$) ${}^4\text{F}$	+	15%	2 (${}^3\text{D}$) ${}^4\text{D}$
68506.23	68423.34	82.89	14	0.05	1.017	42%	1 (${}^1\text{D}$) ${}^2\text{F}$	+	17%	1 (${}^3\text{F}$) ${}^2\text{F}$	+	12%	1 (${}^3\text{P}$) ${}^4\text{D}$
66310.48	66163.44	147.04	13	0.06	1.174	19%	1 (${}^3\text{F}$) ${}^2\text{D}$	+	18%	2 (${}^3\text{D}$) ${}^2\text{D}$	+	18%	2 (${}^3\text{D}$) ${}^4\text{F}$
64053.56	64104.16	-50.60	17	0.06	1.068	39%	1 (${}^3\text{F}$) ${}^2\text{F}$	+	11%	1 (${}^3\text{P}$) ${}^2\text{D}$	+	10%	1 (${}^3\text{P}$) ${}^4\text{D}$
62443.23	62369.28	73.95	14	0.07	1.195	44%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	18%	1 (${}^1\text{D}$) ${}^2\text{F}$	+	14%	1 (${}^3\text{F}$) ${}^4\text{F}$
57606.26	57719.31	-113.05	11	0.05	0.967	47%	1 (${}^3\text{F}$) ${}^4\text{F}$	+	18%	1 (${}^3\text{F}$) ${}^4\text{G}$	+	10%	1 (${}^1\text{D}$) ${}^2\text{D}$
55389.15	55411.72	-22.57	13	0.08	1.026	26%	1 (${}^3\text{F}$) ${}^4\text{D}$	+	19%	1 (${}^3\text{F}$) ${}^2\text{D}$	+	16%	1 (${}^3\text{F}$) ${}^4\text{G}$
48197.85	48248.80	-50.95	7	0.07	0.701	61%	1 (${}^3\text{F}$) ${}^4\text{G}$	+	18%	1 (${}^3\text{F}$) ${}^2\text{F}$	+	13%	1 (${}^1\text{D}$) ${}^2\text{F}$
<i>J = 3.5</i>													
101320.98	101223.30	97.68	10	0.15	1.145	56%	2 (${}^3\text{D}$) ${}^2\text{F}$	+	27%	2 (${}^1\text{D}$) ${}^2\text{F}$	+	9%	1 (${}^1\text{G}$) ${}^2\text{F}$
89634.08	89607.09	26.99	6	0.13	1.156	57%	2 (${}^1\text{D}$) ${}^2\text{F}$	+	24%	2 (${}^3\text{D}$) ${}^2\text{F}$	+	8%	1 (${}^1\text{D}$) ${}^2\text{F}$
78623.20	78596.68	26.52	10	0.07	1.338	58%	2 (${}^3\text{D}$) ${}^4\text{D}$	+	12%	1 (${}^3\text{P}$) ${}^4\text{D}$	+	9%	1 (${}^1\text{G}$) ${}^2\text{F}$
77805.32	77952.34	-147.02	15	0.06	1.137	46%	1 (${}^1\text{G}$) ${}^2\text{F}$	+	18%	1 (${}^1\text{G}$) ${}^2\text{G}$	+	13%	2 (${}^3\text$

Table III. *Continued.*

E_{obs}	E_{calc}	Δ^{a}	N^{b}	rms	g^{c}	Composition ^d
<i>J = 4.5</i>						
80061.85	80151.54	-89.69	7	0.08	1.334	98% 2 (${}^3\text{D}$) ${}^4\text{F}$ + 1% 1 (${}^3\text{F}$) ${}^4\text{F}$ + 1% 1 (${}^1\text{G}$) ${}^2\text{G}$
75519.76	75563.05	-43.29	7	0.07	1.033	56% 1 (${}^1\text{G}$) ${}^2\text{G}$ + 41% 1 (${}^1\text{G}$) ${}^2\text{H}$ + 2% 1 (${}^3\text{F}$) ${}^4\text{F}$
72393.26	72368.12	25.14	11	0.09	1.092	65% 1 (${}^3\text{F}$) ${}^2\text{G}$ + 17% 1 (${}^1\text{G}$) ${}^2\text{H}$ + 12% 1 (${}^1\text{G}$) ${}^2\text{G}$
68136.41	68089.50	46.91	10	0.09	1.133	41% 1 (${}^3\text{F}$) ${}^4\text{F}$ + 35% 1 (${}^1\text{G}$) ${}^2\text{H}$ + 16% 1 (${}^3\text{F}$) ${}^2\text{G}$
63339.06	63346.79	-7.73	10	0.05	1.201	34% 1 (${}^3\text{F}$) ${}^4\text{F}$ + 32% 1 (${}^3\text{F}$) ${}^4\text{G}$ + 19% 1 (${}^3\text{F}$) ${}^2\text{G}$
58907.94	58846.52	61.42	8	0.06	1.179	68% 1 (${}^3\text{F}$) ${}^4\text{G}$ + 15% 1 (${}^3\text{F}$) ${}^4\text{F}$ + 9% 1 (${}^3\text{F}$) ${}^2\text{G}$
<i>J = 5.5</i>						
77747.11	77694.68	52.43	4	0.05	1.098	96% 1 (${}^1\text{G}$) ${}^2\text{H}$ + 4% 1 (${}^3\text{F}$) ${}^4\text{G}$
65531.18	65639.20	-108.02	3	0.05	1.267	96% 1 (${}^3\text{F}$) ${}^4\text{G}$ + 4% 1 (${}^1\text{G}$) ${}^2\text{H}$

^a $\Delta = (E_{\text{obs}} - E_{\text{calc}})$.^b N = The number of spectral lines used to determine the energy level value.^c g = The calculated Landé factor.^d The number preceding the term name has the following meaning: 1 stands for $5\text{d}^26\text{p}$, 2 stands for $5\text{d}6\text{s}6\text{p}$, and 3 stands for $6\text{s}^26\text{p}$.Table IV. Least-squares fitted (LSF) and calculated parameter values (cm^{-1}) in the 5d^3 , $5\text{d}^26\text{s}$ and $5\text{d}6\text{s}^2$ configurations of Ta III.

Parameter	LSF	HFR	LSF/HFR
5d³			
E_{av}	15729.9 (32.4)	19061.4	
O_2	4508.7 (36.9)	5788.7	0.7789
O'_2	3197.7 (27.6)	4005.1	0.7984
E_a	94.9 (28.1)		
E_b	39.1 (40.0)		
ζ_d	1909.4 (18.7)	2141.2	0.8917
A_c	21.6		
A_3	2.4		
A_4	4.2		
A_5	4.3		
A_6	11.7		
A_1	-1.8		
A_2	2.0		
A_0	-1.6		
5d²6s			
E_{av}	19548.8 (32.0)	24121.0	0.7548 ^a
O_2	4766.1 (25.8)	6058.0	0.7868
O'_2	3428.9 (35.2)	4171.9	0.8219
E_a	106.6 (41.6)		
E_b	-10.0		
ζ_d	2105.6 (23.4)	2327.2	0.9048
A_c	20.9		
A_3	2.4		
A_4	4.2		
A_5	4.2		
A_6	11.3		
A_1	-1.7		
A_2	1.9		
A_0	-1.5		
C_{ds}	2796.0 (26.5)	3714.0	0.7528
T_{dds}	17.5 (33.7)		
A_{mso}	49.8 (20.3)		
5d6s²			
E_{av}	33115.3 (270.3)	42313.2	0.7477 ^a
ζ_d	2310.8 (79.4)	2519.3	0.9172
$R^2(\text{dd}, \text{ds})12^b$	-20343.1 (134.9)	-26263.6	0.7746
$R^2(\text{dd}, \text{ss})12$	17141.8 (212.0)	23949.6	0.7157
$R^2(\text{dd}, \text{ds})23$	-19846.7 (878.7)	-26271.8	0.7554
Mean Deviation ^c = 70 cm^{-1}			

^a The energy differences with respect to the ground configuration were used: $(E_{\text{av}}(\text{conf}) - E_{\text{av}}(5\text{d}^3))_{\text{LSF}} / (E_{\text{av}}(\text{conf}) - E_{\text{av}}(5\text{d}^3))_{\text{HFR}}$, where “conf” is either $5\text{d}^26\text{s}$ or $5\text{d}6\text{s}^2$.^b “xy” behind the R -integral means interaction between configuration x and y . 1 stands for 5d^3 , 2 stands for $5\text{d}^26\text{s}$ and 3 stands for $5\text{d}6\text{s}^2$.^c Mean Deviation = $[(\sum(E_{\text{obs}} - E_{\text{calc}})^2) / (n - m)]^{1/2}$, where n is the number of known levels, m is the number of free parameters.

Table V. Least-squares fitted (LSF) and calculated parameter values (cm^{-1}) in the $5d^26p$, $5d6s6p$ and $6s^26p$ configurations of Ta III.

Parameter	LSF	HFR	LSF/HFR
5d²6p			
E_{av}	68808.2 (52.3)	71171.4	1.0186 ^a
O_2	4719.3 (60.0)	6149.5	0.7674
O'_2	3491.0 (47.3)	4227.9	0.8257
E_a	10.7 (78.9)		
E_b	-91.7 (61.0)		
ζ_d	2245.4 (26.5)	2386.4	0.9409
A_c	21.6		
A_3	2.4		
A_4	4.2		
A_5	4.3		
A_6	11.7		
A_1	-1.8		
A_2	2.0		
A_0	-1.6		
$C_1(\text{dp})$	1899.7 (52.9)	2301.3	0.8255
$C_2(\text{dp})$	2100.0 (62.8)	2907.1	0.7224
$C_3(\text{dp})$	1286.6 (48.3)	1628.8	0.7899
$S_1(\text{dp})$	239.9 (57.5)		
$S_2(\text{dp})$	-112.7 (42.8)		
T_{16}	-25.0		
T_{25}	5.0		
T_{26}	-35.0		
T_{27}	5.0		
T_{28}	55.0		
T_{29}	-35.0		
T_{30}	10.0		
ξ_p	5390.0 (59.0)	4467.4	1.2065
SS_{02}	0.0		
SS_{20}	0.0		
$S_d \cdot L_p$	-90.0		
$S_p \cdot L_d$	-10.0		
Z_{pp}^2	-50.0		
Z_{dd}^2	60.0		
Z_{pl}^2	100.0		
Z_{ld}^2	0.0		
Z_{p}^3	40.0		
Z_{dd}^3	-30.0		
5d6s6p			
E_{av}	81729.0 (116.3)	85349.8	0.9956 ^a
ζ_d	2536.7 (58.1)	2573.1	0.9859
Cd_s	2904.2 (144.4)	3672.4	0.7908
A_{mso}	52.0		
A_{ss}	0.0		
$C_1(\text{dp})$	2430.1 (83.0)	2483.7	0.9784
$C_2(\text{dp})$	2213.3 (94.0)	2952.9	0.7495
$C_3(\text{dp})$	1623.2 (82.4)	1626.6	0.9979
$S_1(\text{dp})$	-75.6 (66.9)		
$S_2(\text{dp})$	-150.7 (140.6)		
ζ_p	5554.0 (213.6)	5210.3	1.0660
$S_d \cdot L_p$	-90.0		
$S_p \cdot L_d$	-10.0		
Z_{pp}^2	-50.0		
Z_{dd}^2	60.0		
Z_{pl}^2	100.0		
Z_{ld}^2	0.0		
Z_{p}^3	40.0		
Z_{dd}^3	-30.0		
C_{sp}	6871.7 (118.6)	11446.6	0.6003
$A_{\text{mso}}(\text{sp})$	-615.5 (265.7)		
6s²6p			
E_{av}	105500.0	113571.7	0.9498 ^a
ζ_p	7165.0	6021.2	1.1900
$R^2(\text{dd}, \text{ds})12^b$	-21787.2 (792.2)	-26215.3	0.8311
$R^2(\text{dp}, \text{sp})12$	-14751.3 (435.1)	-21442.2	0.6880
$R^1(\text{dp}, \text{ps})12$	-14024.5 (341.5)	-20439.8	0.6861
$R^2(\text{dd}, \text{ss})13$	16744.0	23728.5	0.7056
$R^2(\text{dp}, \text{sp})23$	-15495.0	-21957.7	0.7057

Table V. *Continued.*

Parameter	LSF	HFR	LSF/HFR
$R^1(\text{dp, ps})_{23}$	-14664.0	-20780.0	0.7057

Mean Deviation^c = 126 cm⁻¹^a The energy differences with respect to the ground configuration were used: $(E_{\text{av}}(\text{conf}) - E_{\text{av}}(5d^3))_{\text{LSF}} / (E_{\text{av}}(\text{conf}) - E_{\text{av}}(5d^3))_{\text{HFR}}$, where “conf” is either 5d²6p, 5d6s6p or 6s²6p.^b “xy” behind the R -integral means interaction between configuration x and y . 1 stands for 5d²6p, 2 stands for 5d6s6p and 3 stands for 6s²6p.^c Mean Deviation = $[(\sum(E_{\text{obs}} - E_{\text{calc}})^2) / (n - m)]^{1/2}$, where n is the number of known levels, m is the number of free parameters.

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